

Simulation Tools to Study Distribution Systems Including Distributed Generation and Practical Case Studies in Canada

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POWER ENGINEERING SOFTWARE SOLUTIONS



CYME
INTERNATIONAL T&D

Overview

- **Introduction**
- **CYME-NRCan Collaboration**
- **Utility Survey and Current Status**
- **CYMDIST Enhancements**
- **Case Studies – Demonstration/Tutoring**
- **Conclusions**

Introduction

- **The benefits of installing DGs in distribution networks have already been established**
- **There are several pitfalls to their application to existing distribution systems**
- **Interaction between DGs and the distribution system involves several phenomena that need thorough investigation**
- **There is a need for enhanced analysis tools for distribution systems as well as the development of engineering skills in using them**

NRCan – CYME collaboration



CYME/NRCan DG software approach

- 1. Industry survey**
 - Identify gaps
- 2. CYMDIST software enhancements**
 - Add DG models
 - Add dynamic functionalities
 - Add planned islanded network option
- 3. Knowledge transfer**
 - Case studies for training/tutorial material
 - Educate – DG issues, relevant standards, new modeling features

Utility Survey and Current Status

- A survey of 30 distribution utilities representing 9 provinces and 2 territories serving over 7million customers was conducted by CYME on behalf of NRCan
- The main objectives of the survey were to:
 - Establish distribution engineers experience and adequacy of analytical tools at their disposal for conduction of DG integration studies
 - Provide insight into the direction distribution planning is heading and its effect on the need for special skills and enhanced tools.

Utility Survey and Current Status (Cont.)

The survey results indicated that:

- Major enhancement of current analytical tools is necessary for handling emerging technology in distribution systems
- Increasing distribution engineers familiarity with and ability to handle state of the art is essential
- CYMDIST is the most widely used distribution analysis tool among Canadian engineers

CYME - NRCan Collaboration Plan

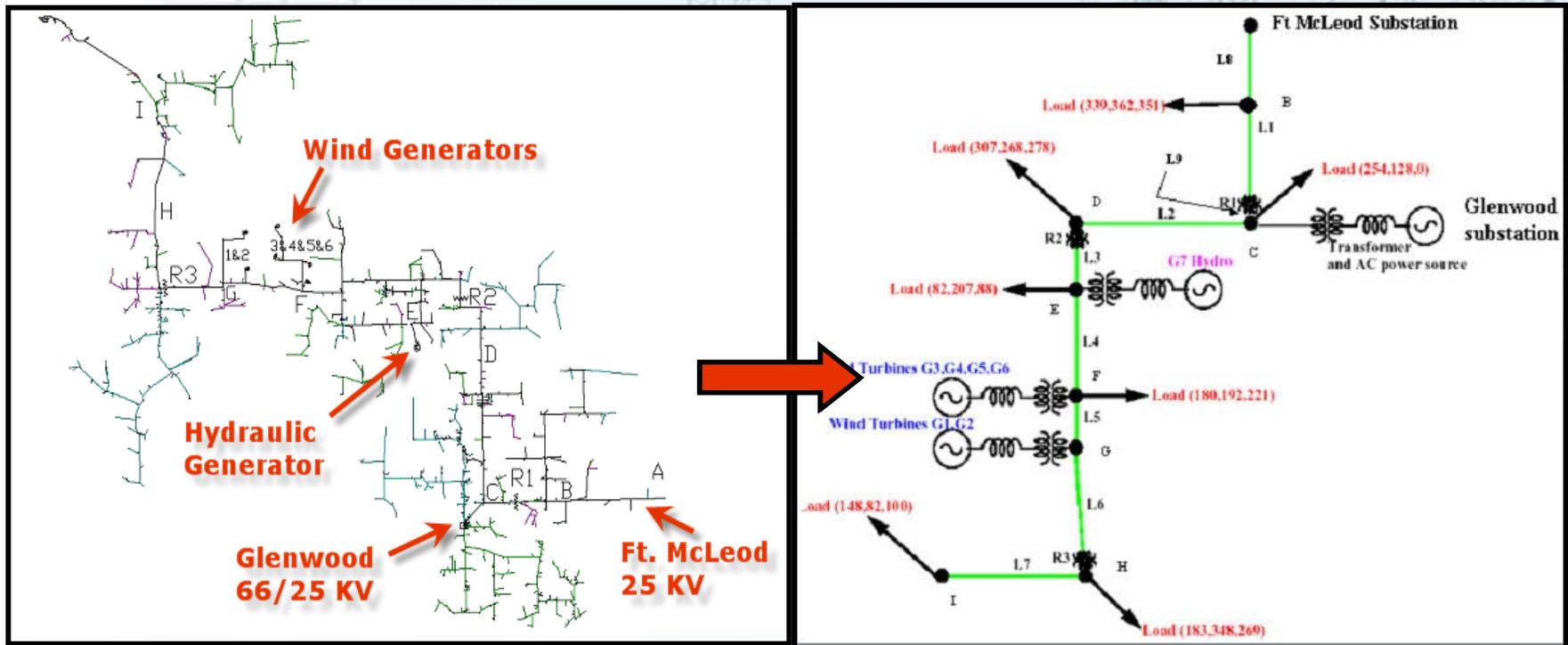
- A collaboration plan between CYME and NRCan Was developed
- The primary objectives of the project are:
 - To add feature to CYMDIST to simplify the use of the program for DG interface studies
 - To implement the most common DG models in CYMDIST and provide adequate means to investigate the impact of DG on distribution networks
- The plan is being implemented in three phases

Phase I – Steady State Analysis

- Create a library of typical data for DG units in the form of look-up tables or estimation functions
- Provide the ability to simulate isolated distribution systems with embedded generation
- Provide the capability of automated network reduction for easier evaluation of DG integration studies
- Create Test Cases of typical systems involving DG for testing different steady state phenomena

The System Reduction Concept

- System reduction concept is demonstrated in the following figure



Phase II – Dynamic Analysis

- Implement, in CYMDIST, dynamic models of system components involved in transient stability and frequency behavior studies
- Provide ability to simulate events such as faults, load and generation rejection, component tripping, etc.
- Provide the ability to report and monitor different variables during the dynamic simulation
- Create Test Cases of typical systems to be used for testing dynamic behavior of DS systems

Phase III – Additional DG Models

- Add models of electronically-interfaced DGs:
 - Micro-turbine generation systems
 - Variable-speed wind energy systems:
 - Direct drive synchronous generator
 - Direct drive permanent magnet generator
 - Doubly-fed induction generator
 - Photovoltaic systems
 - Fuel cell systems
 - Battery energy storage systems

Phase III – Additional DG Models (Cont.)

- **Develop dynamic models of small DG units of conventional technologies:**
 - **Combined cycle units**
 - **Kaplan turbine hydraulic units**
- **Implement protective functions relevant to distribution systems with embedded DG resources.**
- **Develop typical distribution system with DG units and set up test cases to illustrate system/unit dynamic interaction**

Case studies - objectives

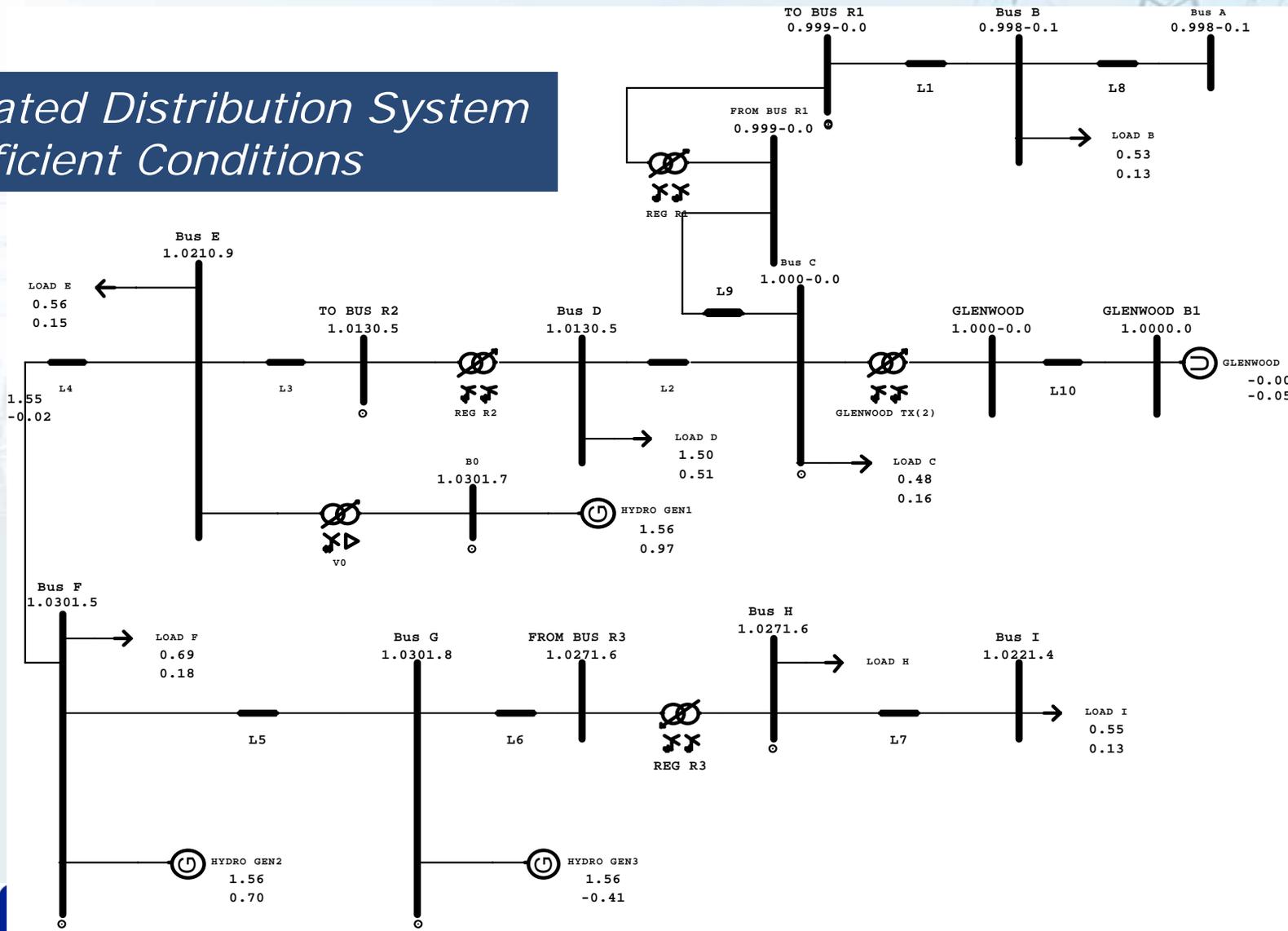
- To demonstrate the effect of distributed resources on steady-state and dynamic behavior of distribution systems
- Education and dissemination of information
- The study cases demonstrate the response of the system to disturbances and the effect of:
 - Type of embedded generation
 - Operating conditions
 - Degree of penetration of the DG resources

Distribution system modeled

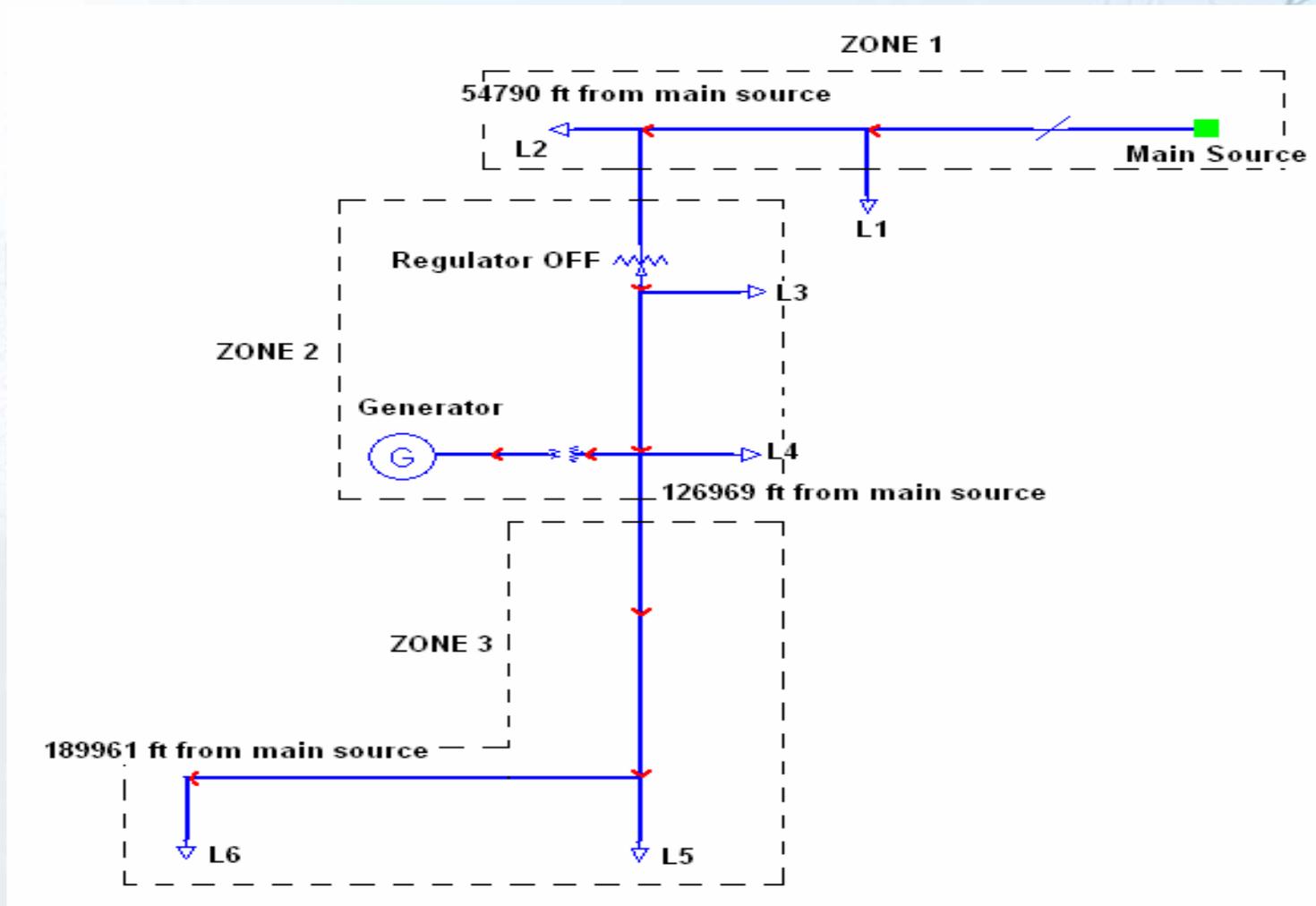
- **Actual 25 kV multi-grounded distribution circuit with several laterals feeding multiple loads.**
- **The distribution system is connected to the main power system at bus bar B1.**
- **DG units, of varying types and sizes are connected to bus bars B0, F and G. Loads are connected to bus bars B, C, D, E, F, H and I.**
- **Total load is 4.627 MW +1.313 MVAR, the largest is 1.5 MW +0.51 MVAR connected to bus bar B.**

Distribution System Modeled (cont.)

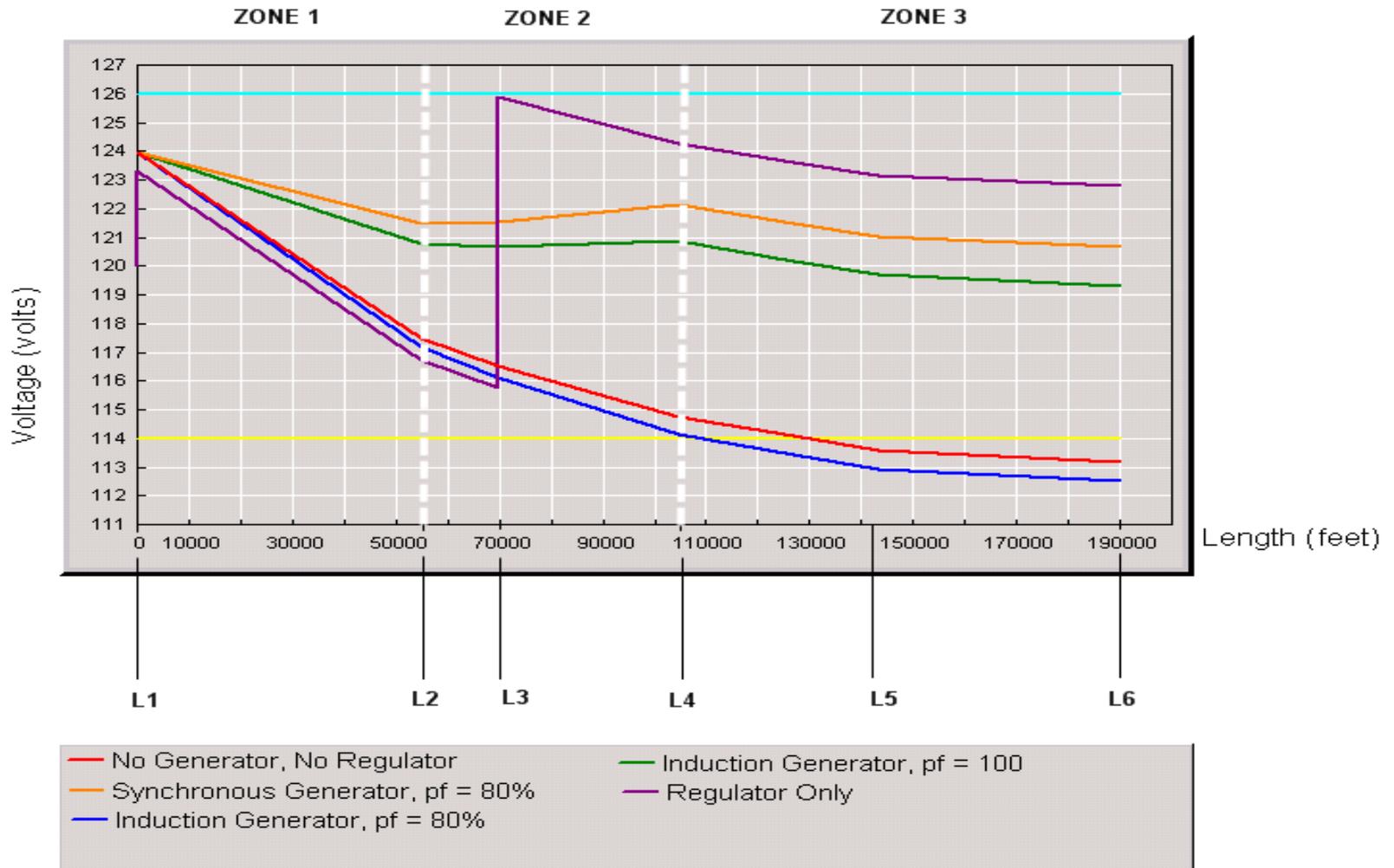
Investigated Distribution System Self-Sufficient Conditions



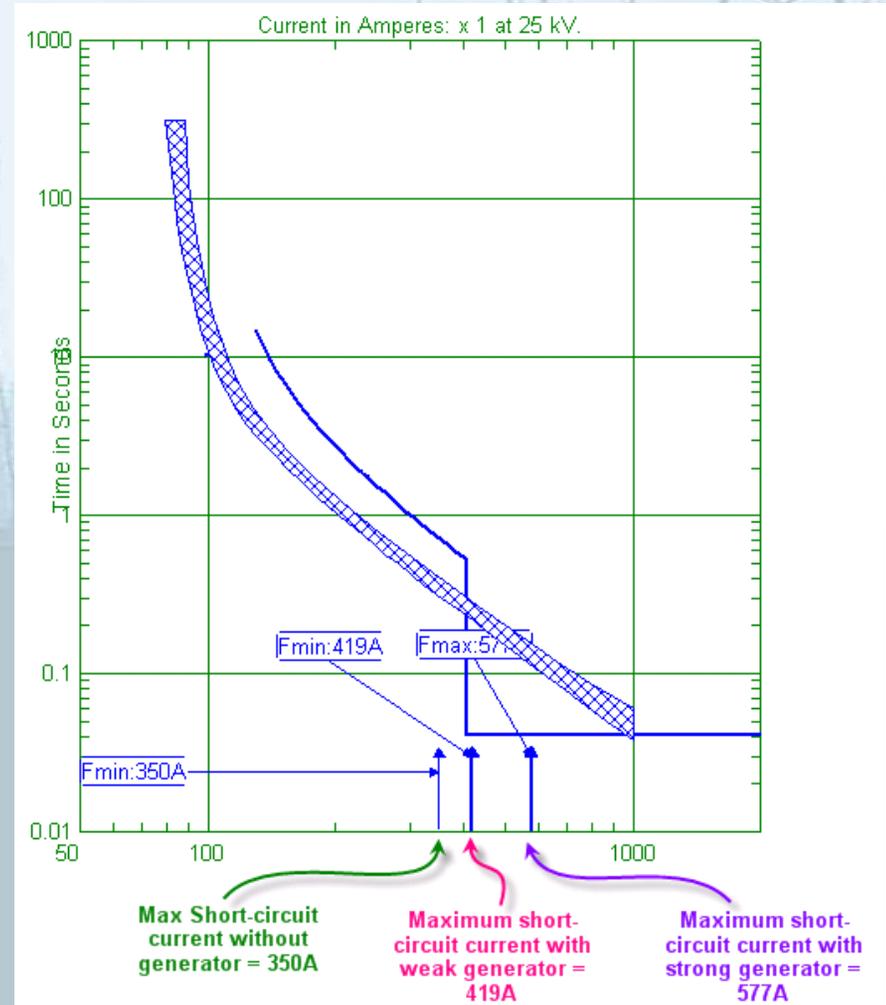
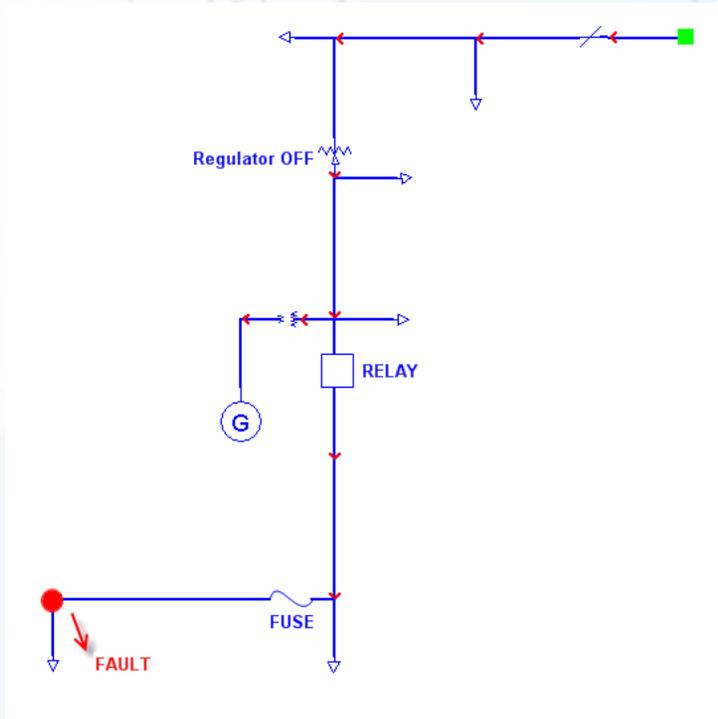
Phase I - Voltage profile analysis



Phase I - Voltage profile analysis (Cont.)



Phase I - Protection coordination study



Phase II - Dynamic Models of Component

■ The following components models were used:

- Load model
- Generator models
- Excitation system model
- Prime mover models
- Wind turbine model
- IEEE Anti-Islanding Standards

Load Model

- Load composition is reflected in its dependence on system voltage and frequency:

$$P = P_o \times (V_{pu})^{n_P} \times [1 + P_{freq} (F_{pu} - 1)]$$

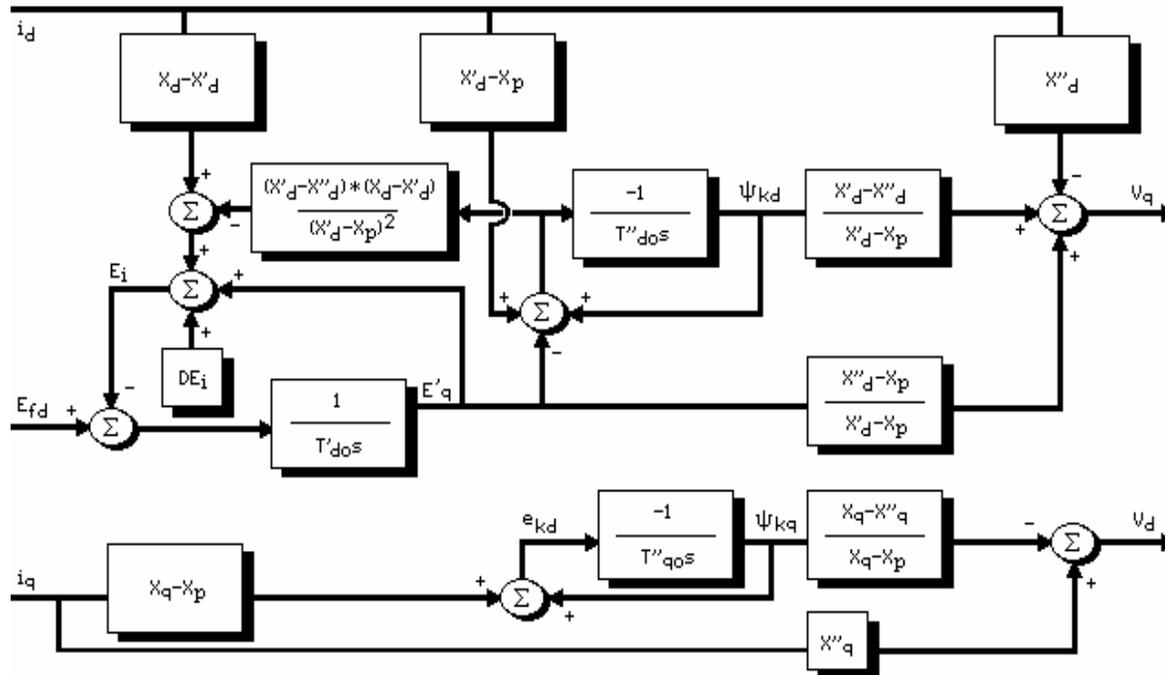
$$Q = Q_o \times (V_{pu})^{n_Q} \times [1 + Q_{freq} (F_{pu} - 1)]$$

- Voltage dependence reflected in n_P and n_Q
- Frequency dependence reflected in P_{freq} and Q_{freq} .

Generator Models

■ Salient pole synchronous generators

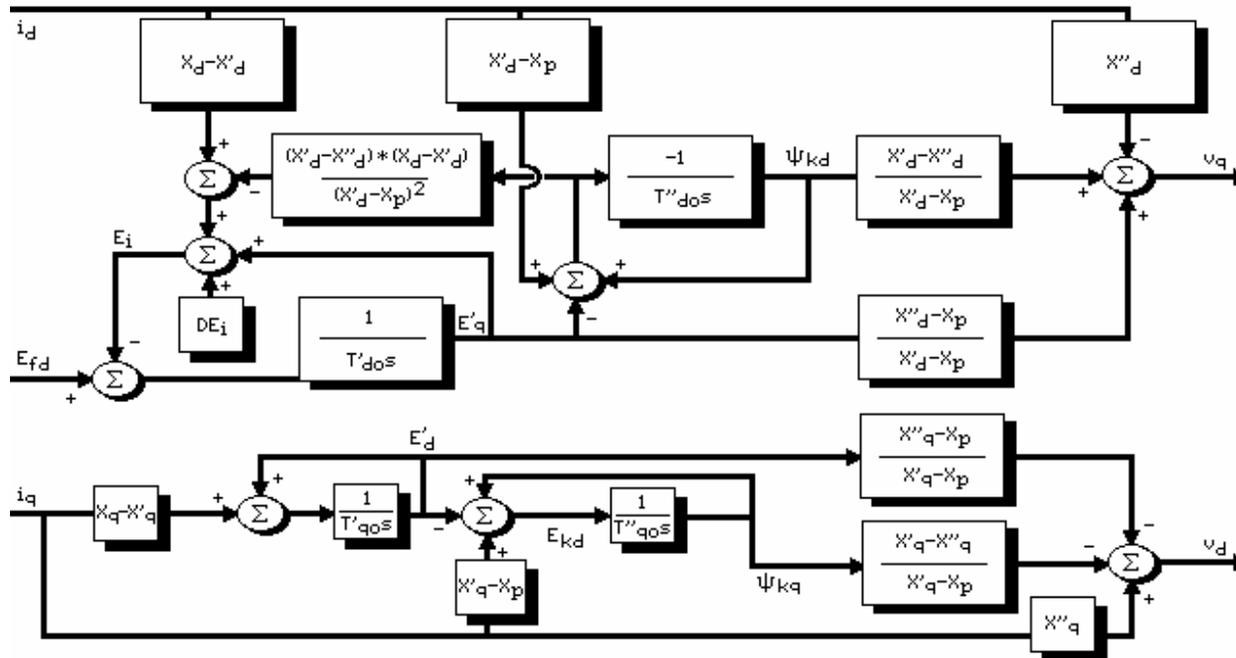
- Used in hydraulic units. Model accounts for saliency, sub-transient response and saturation effects.



Generator Models (cont.)

■ Round rotor synchronous machines

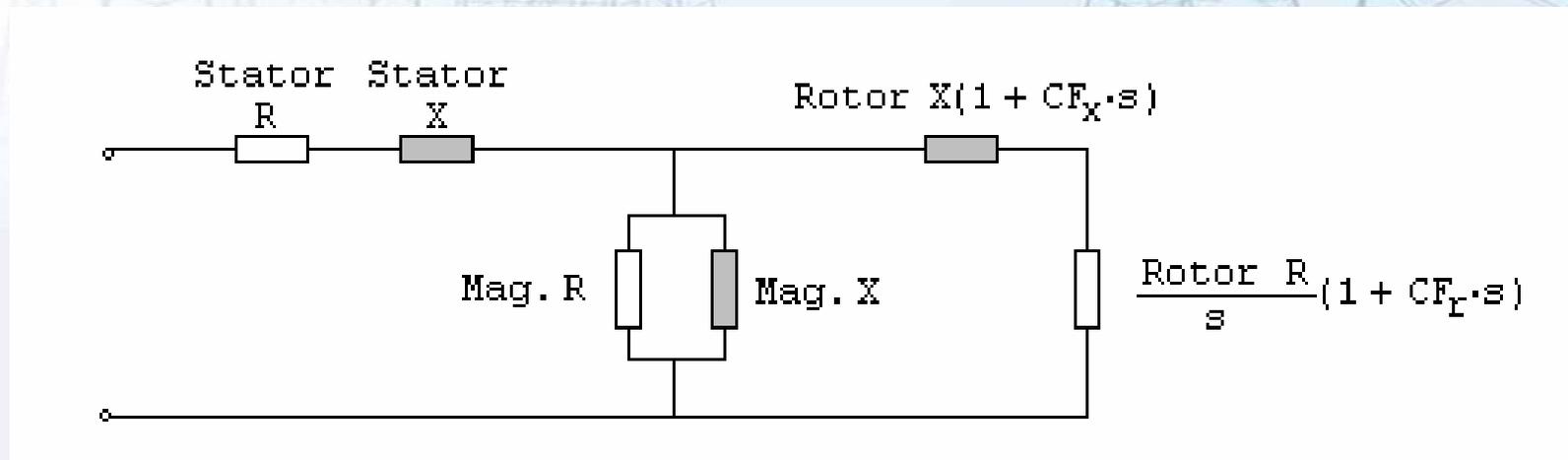
- Used for thermal units. Model accounts for sub-transient and saturation effects.



Generator Models (cont'd)

■ Induction generator model

- Modeled using equivalent electrical circuit

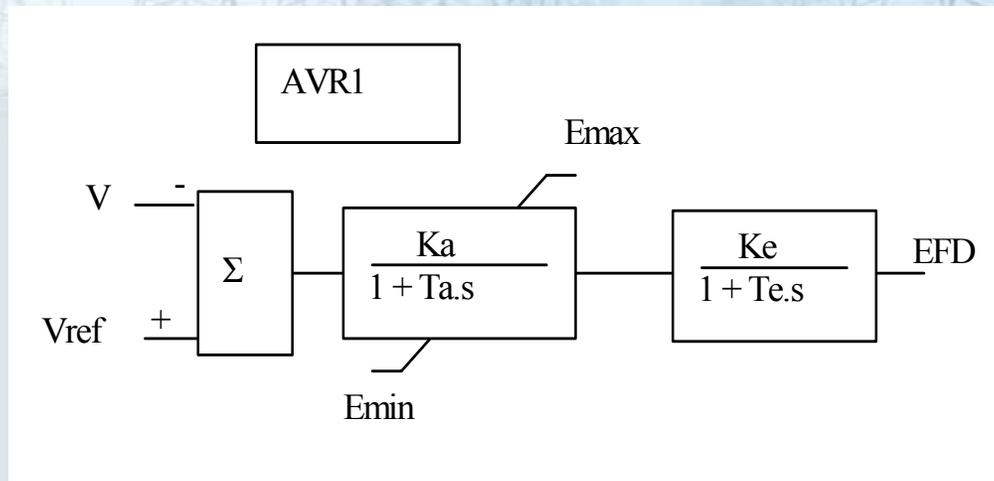


Induction Generator Equivalent Circuit

Excitation System Model

■ Excitation and automatic voltage regulator model

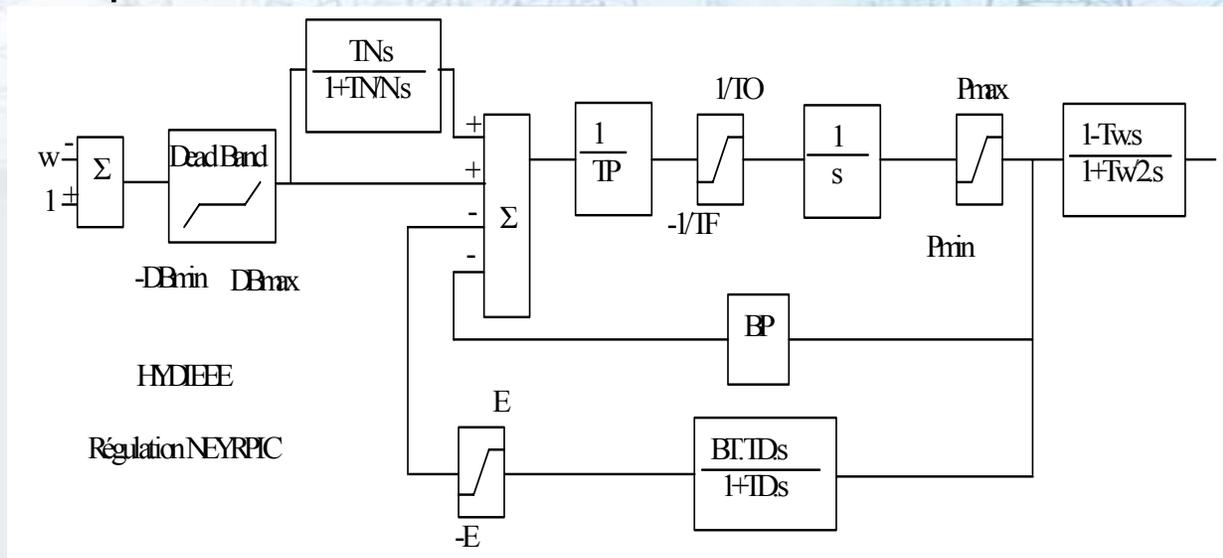
- Used for salient pole and round rotor synchronous generators



Prime Mover Models

■ Hydraulic units

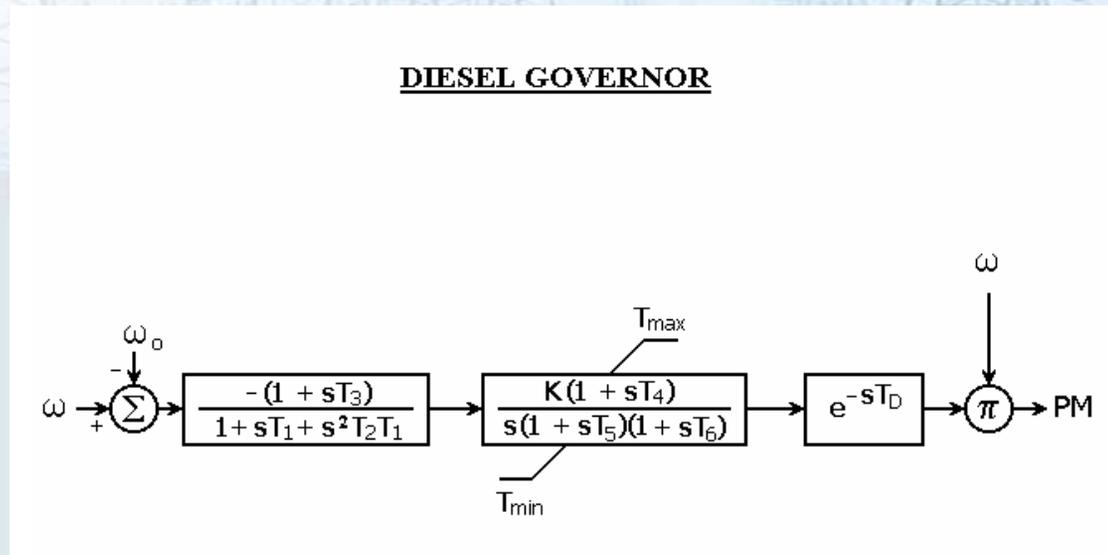
- Hydraulic turbine model reproduces water column dynamics and gate control
- Governor model includes permanent and transient droops



Prime Mover Models (cont.)

■ Diesel units

- Diesel unit governor - fast response - no permanent droop.
- Adjusts unit speed to its set point (60Hz) irrespective of load.

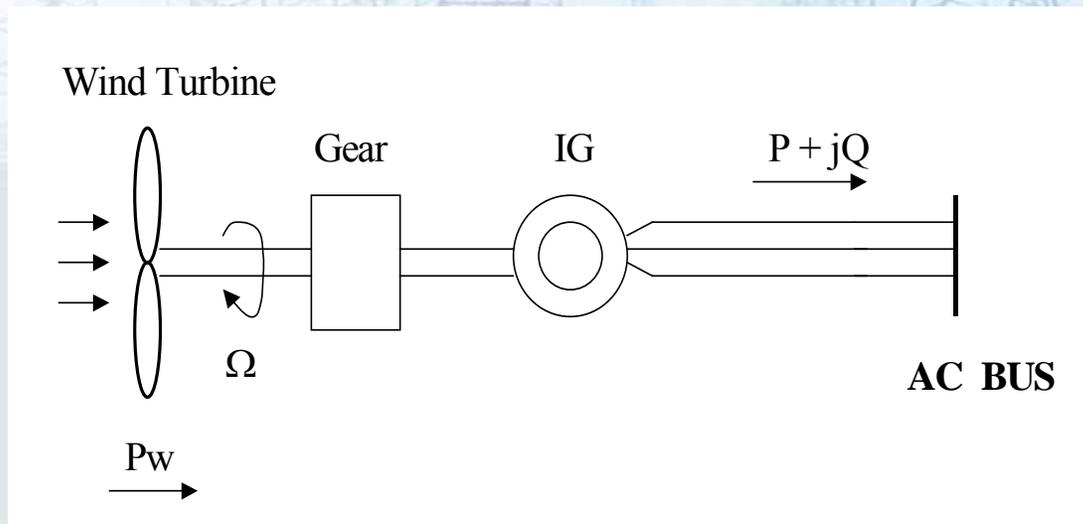


Governor/Turbine Model of a Diesel Engine

Prime Mover Models (cont.)

■ Wind turbine model

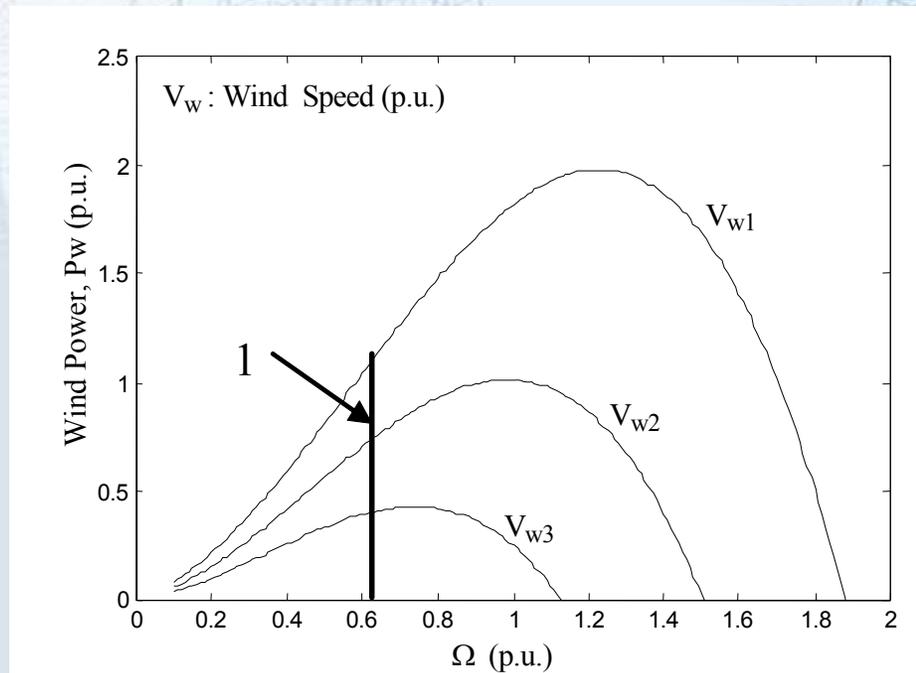
- Directly coupled induction generators driven by wind turbine.



Prime Mover Models (cont.)

■ Wind turbine model

- Operates at roughly constant speed.
- Input wind power is determined entirely by wind speed.



IEEE Anti Islanding Standards

Current IEEE Standards do not allow island operation of distribution systems

■ Voltage limits and clearing times

- When voltage is in specified range, DR disconnects within the clearing times indicated.

Voltage Range (% of base voltage ^a)	Clearing Time ^b (s)
$V < 50$	0.16
$50 \leq V < 88$	2
$110 < V < 120$	1
$V \geq 120$	0.16

Notes.

(a) Base voltages are the nominal system voltages.

(b) DR \leq 30kW, Maximum Clearing Times; DR $>$ 30kW, Default Clearing Times

IEEE Anti Islanding Standards (cont.)

■ Frequency limits and clearing times

- When frequency is in specified range, DR shall disconnect within the clearing times as indicated.

DR SIZE	Frequency Range (Hz)	Clearing Time ^a (s)
≤30 kW	> 60.5	0.16
	<59.3	0.16
>30 kW	>60.5	0.16
	< {59.8 - 57.0} (adjustable set-point)	Adjustable 0.16 to 300
	<57.0	0.16

Note. (a) DR ≤ 30 kW, Maximum Clearing Times; DR > 30 kW, Default Clearing Times

Phase II - Study Cases

- **System response to:**
 - 1. Major disturbances - load or generation rejection – short circuits**
 - 2. Detection of island formation**
 - 3. System operation in island mode**

- **Study cases are repeated for different DG types, mixes and penetration levels.**

Response to Major Disturbances – Case 1

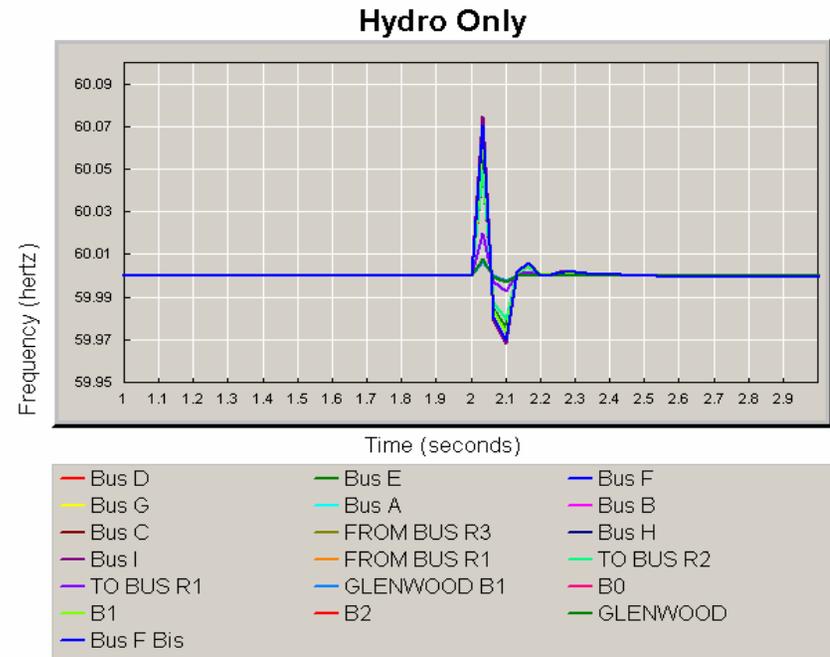
- Response to disturbances not resulting in system separation - load or generation rejection – Sever SCs
- Investigated system conditions:
 - A. Distribution system with hydraulic generation
 - A.1 Self-sufficient distribution system
 - A.2 Over generating distribution system
 - B. Distribution system with wind generation
 - B.1 Self-sufficient distribution system
 - B.2 Over generating distribution system

A. Distribution System with Hydraulic Units

A.1.1 - Loss of load condition

Frequency Response to Load Loss

Balanced Load/Generation
Hydro Units

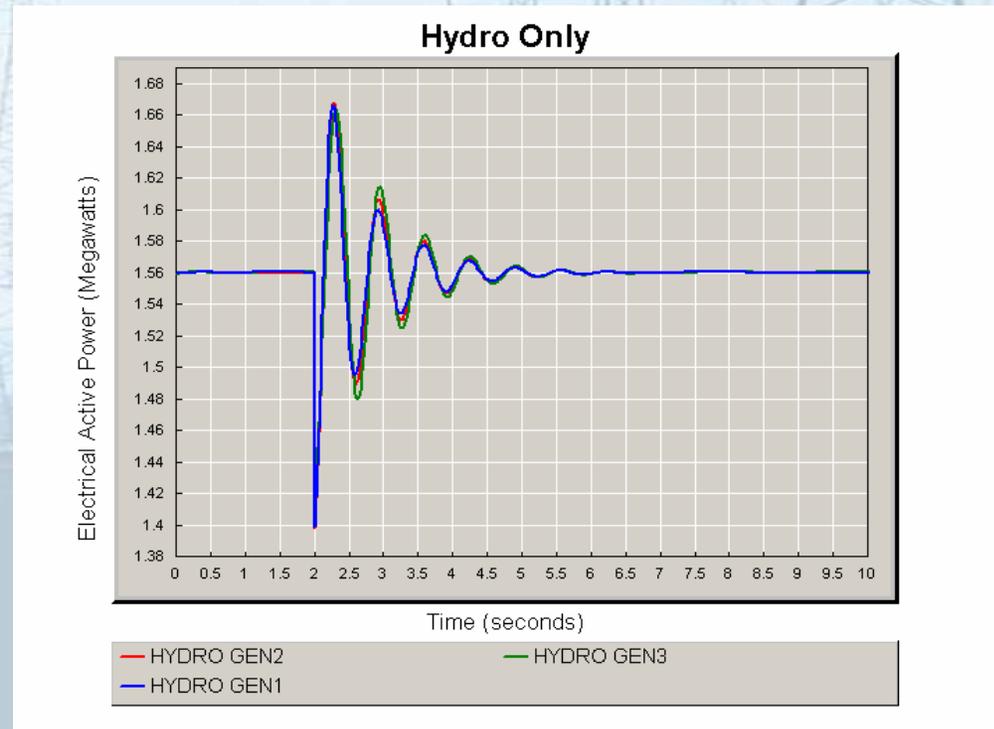


- Frequency returns to its nominal value (60Hz)
- Maximum frequency excursion (60.07 Hz) within IEEE limits

A. Distribution System with Hydraulic Units (cont.)

A.1.1 - Loss of load condition

**Unit Load Response
to Load Loss**
Balanced Load/Generation
Hydro Units



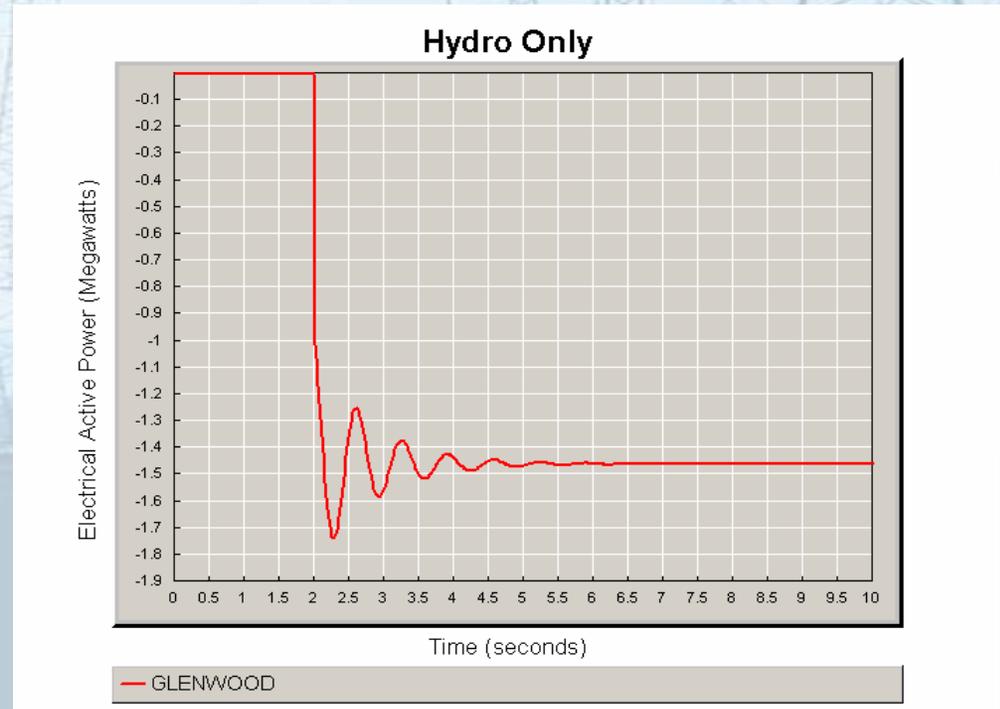
- Generator loads return to their original values

A. Distribution System with Hydraulic Units (cont.)

A.1.1 - Loss of load condition

Transmission System Response to Load Loss

Balanced Load/Generation
Hydro Units

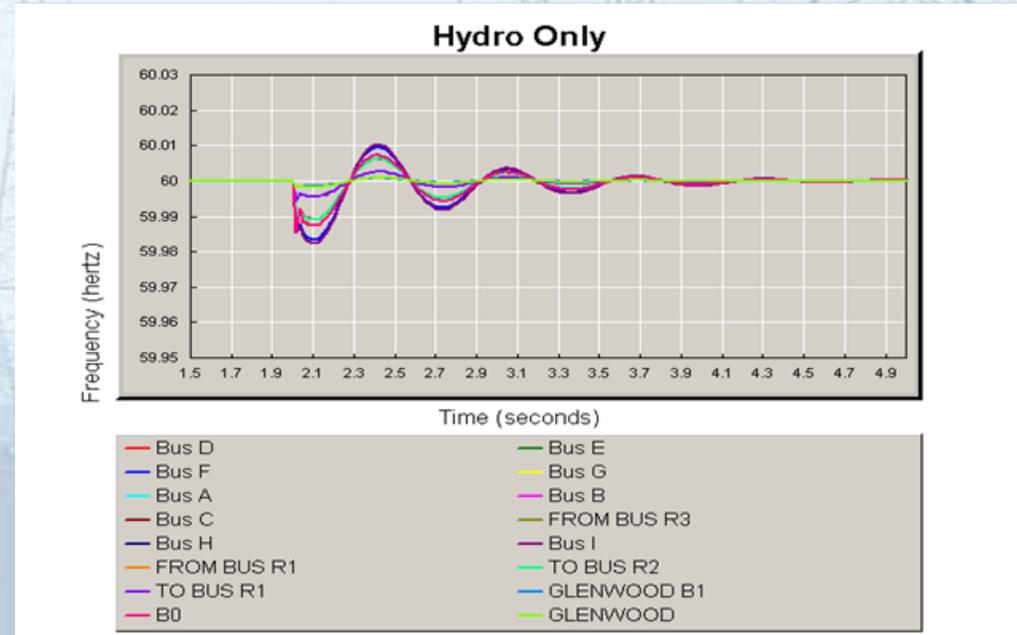


- Feeding system absorbs the excess power

A. Distribution System with Hydraulic Units (cont.)

A.1.2 - Loss of generation condition

**Frequency Response
to Generation Loss**
Balanced Load/Generation
Hydro Units

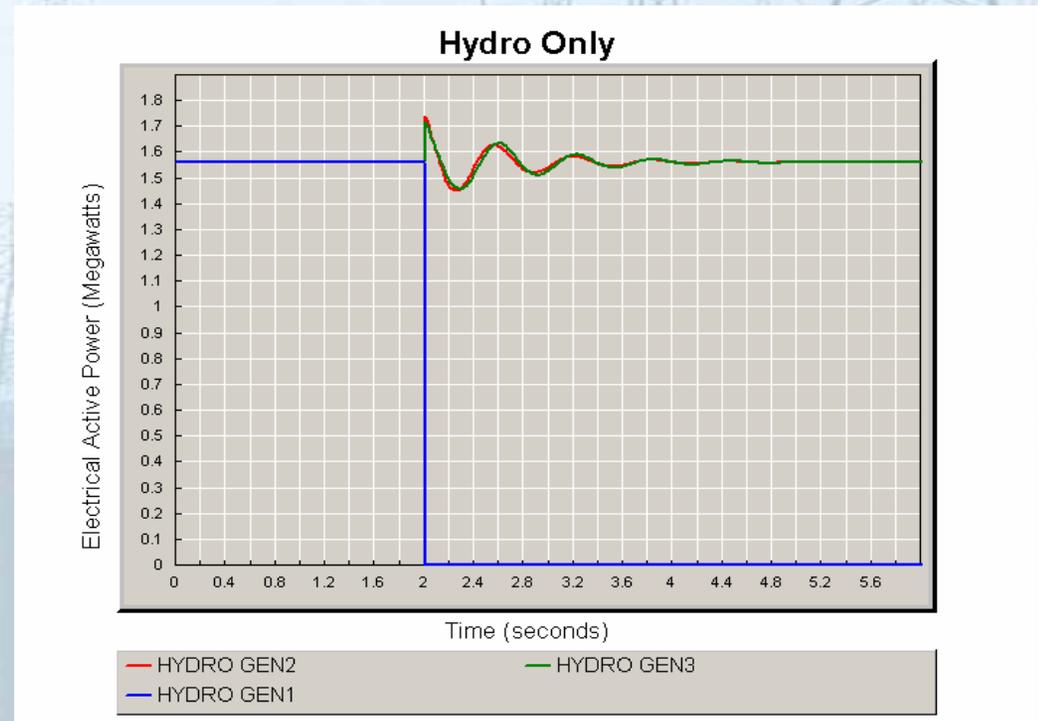


- Frequency returns to its nominal value (60Hz)
- Maximum frequency excursion (59.98 Hz) within IEEE limits

A. Distribution System with Hydraulic Units (cont.)

A.1.2 - Loss of generation condition

**Unit Load Response
to Generation Loss**
Balanced Load/Generation
Hydro Units

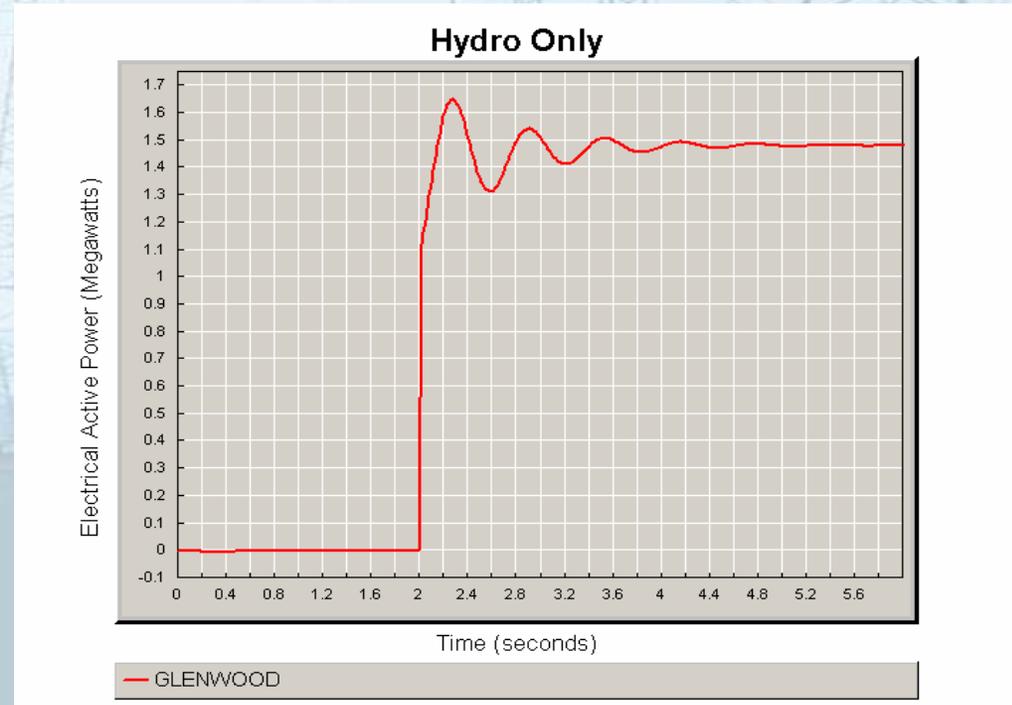


- Generator loads return to their original values

A. Distribution System with Hydraulic Units (cont.)

A.1.2 - Loss of generation condition

**Transmission System
Response to
Generation Loss**
Balanced Load/Generation
Hydro Units



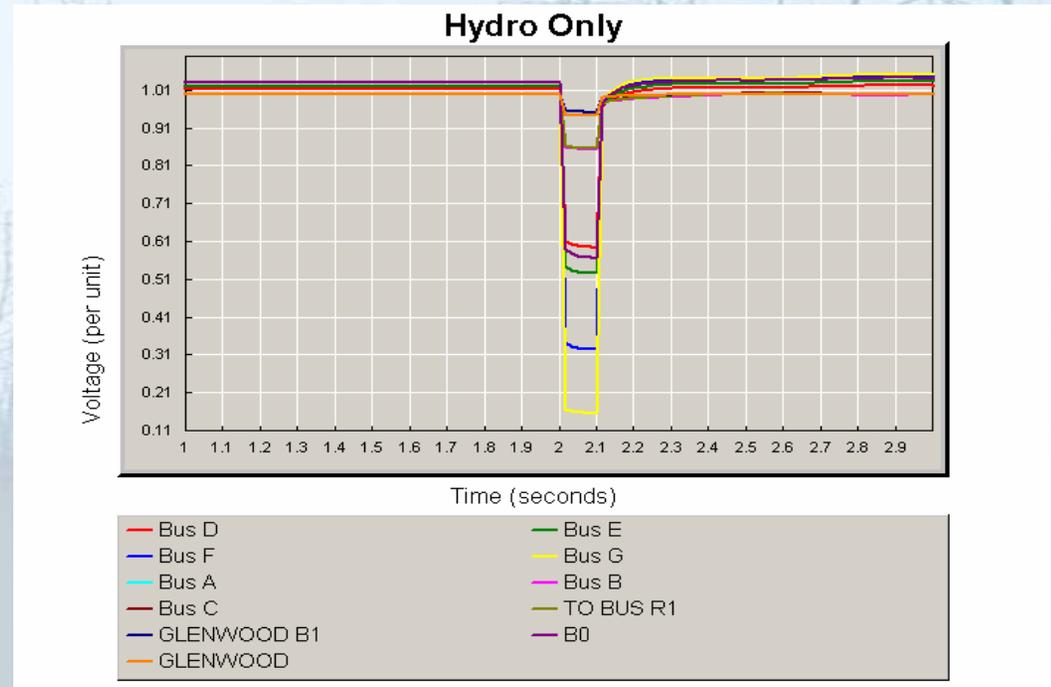
- Feeding system supplies the deficit power

A. Distribution System with Hydraulic Units (cont.)

A.1.3 - Short circuit conditions

Voltage Response to three Phase S.C. at Bus H

Balanced Load/Generation
Hydro Units



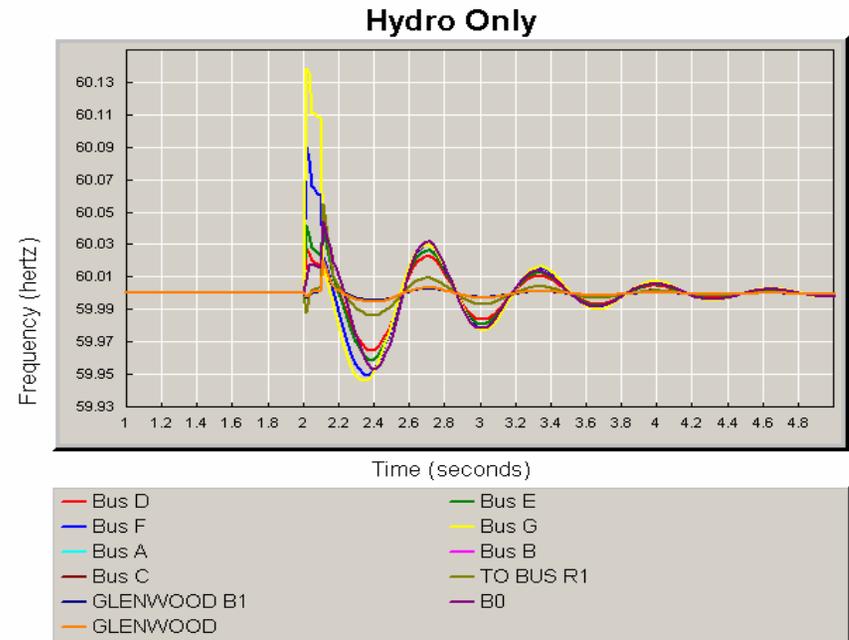
- The voltage dips vary with distance from fault
- The voltages at buses B0, F, and G drop to 0.56 pu, 0.32 pu, and 0.15 pu

A. Distribution System with Hydraulic Units (cont.)

A.1.3 - Short circuit conditions

Frequency Response to three-Phase S.C. at Bus H

Balanced Load/Generation
Hydro Units



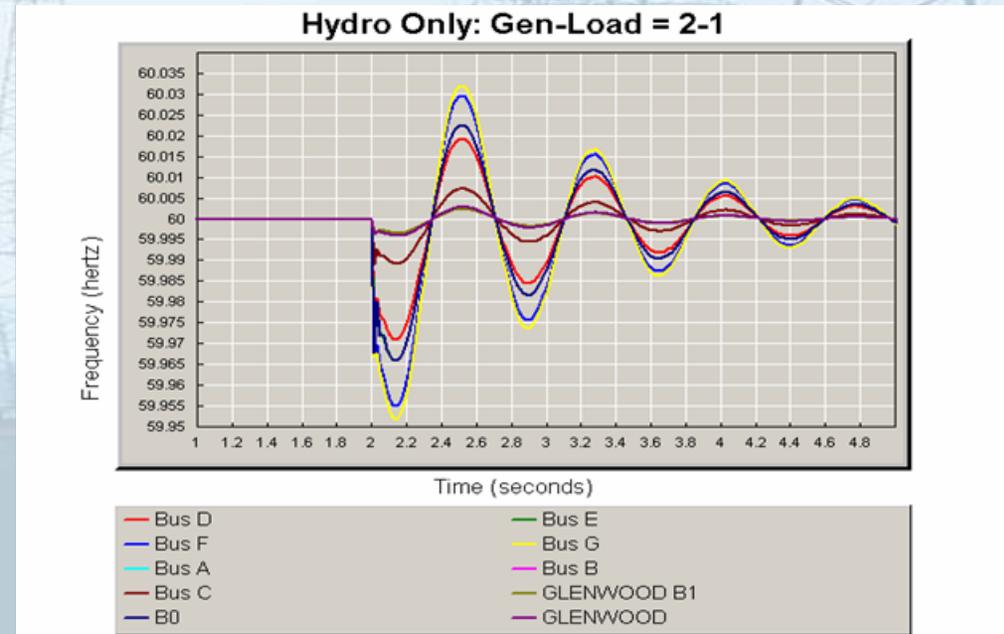
- Frequency returns to its nominal value (60Hz)
- Maximum frequency excursion (60.14 Hz) within IEEE limits

A. Distribution System with Hydraulic Units (cont.)

A.2.1 - Loss of generation condition

Frequency Response to Generation Loss

Generation/Load Ratio 2/1
Hydro Units



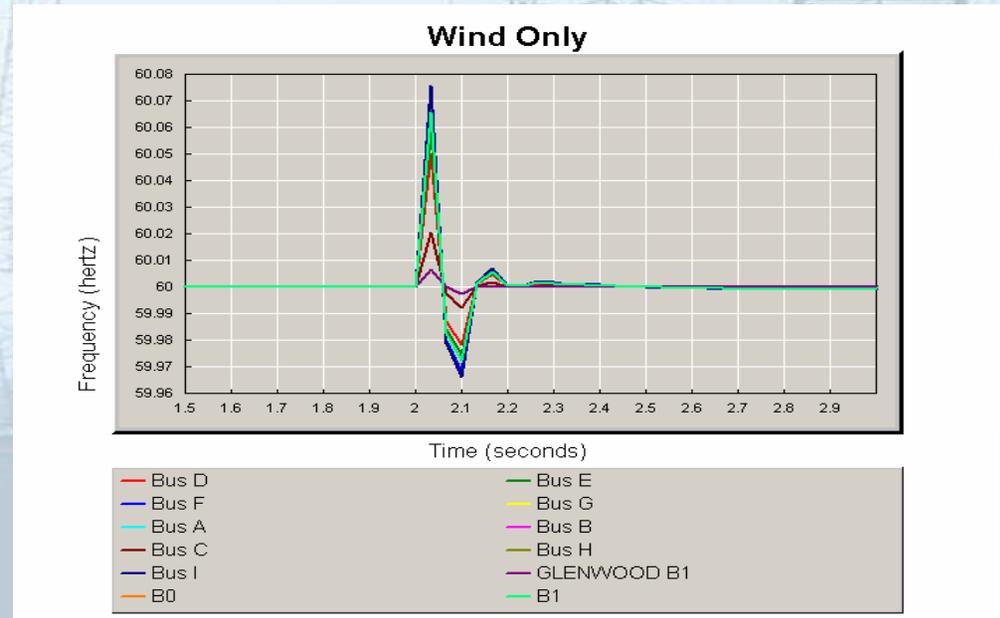
- Frequency returns to its nominal value (60Hz)
- Maximum Frequency excursion (59.95 Hz) within IEEE limits.

B. Distribution System with Wind Units

B.1.1 - Loss of load condition

Frequency Response to Load Loss

Balanced Load/Generation
Wind Units



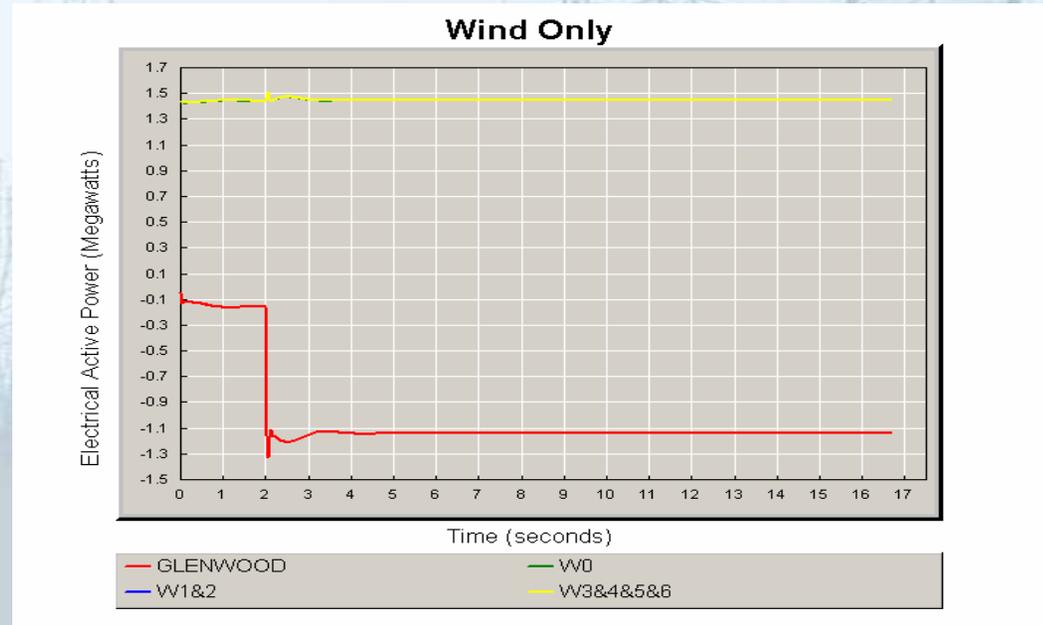
- Frequency returns to its nominal value (60Hz)
- Maximum frequency excursion (60.08 Hz) within IEEE limits

B. Distribution System with Wind Units (cont.)

B.1.1 - Loss of load condition

Generation Response to Load Loss

Balanced Load/Generation
Wind Units

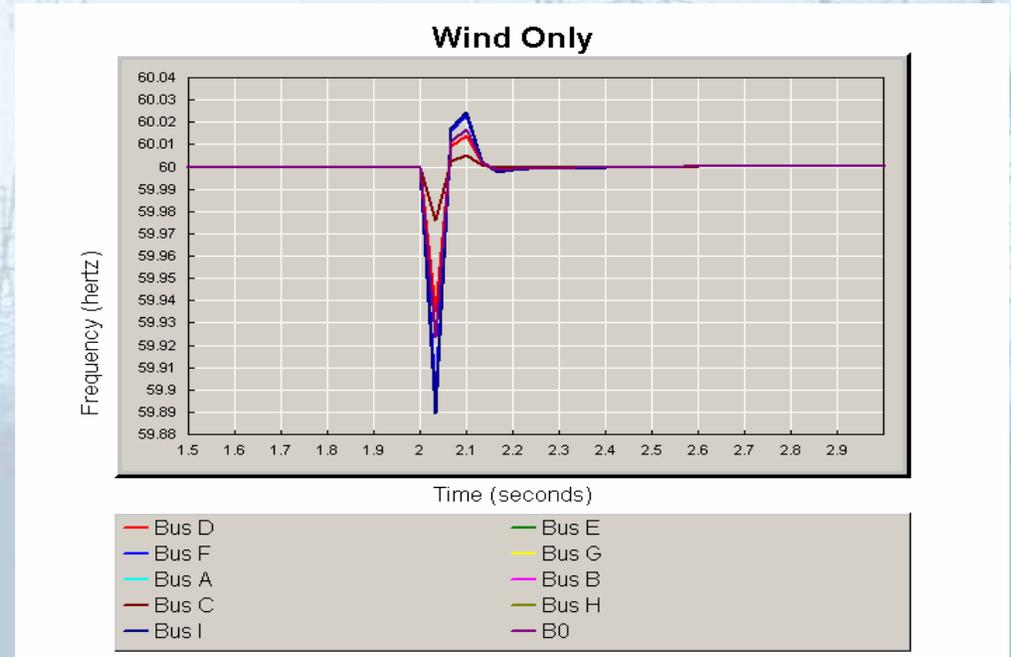


- Wind generation remains constant
- Main system absorbs the excess power

B. Distribution System with Wind Units (cont.)

B.1.2 - Loss of generation condition

**Frequency Response
to Generation Loss**
Balanced Load/Generation
Wind Units

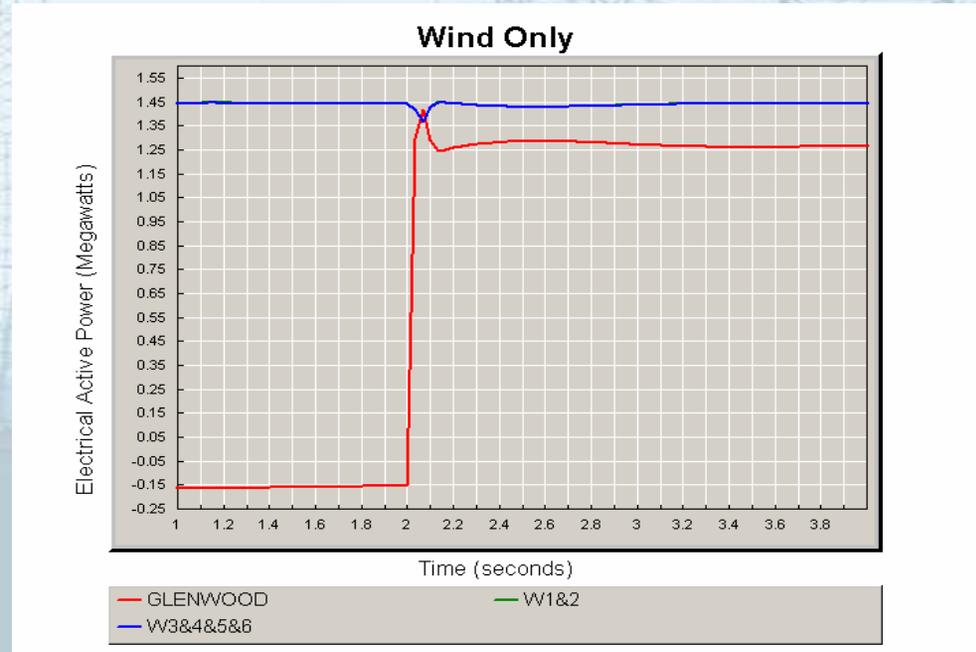


- Frequency returns to its nominal value (60Hz)
- Maximum frequency excursion (59.89 Hz) within IEEE limits

B. Distribution System with Wind Units (cont.)

B.1.2 - Loss of generation condition

**Generation Response
to Generation Loss**
Balanced Load/Generation
Wind Units



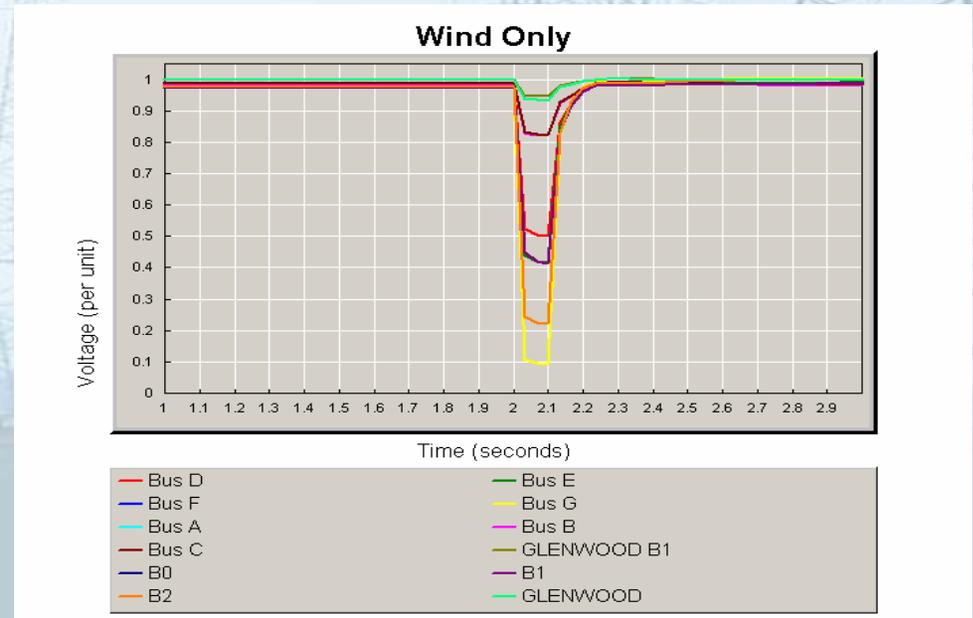
- Wind generation remains constant
- Main system supplies the power deficit

B. Distribution System with Wind Units (cont.)

B.1.3 – Short-circuit condition

Voltage Response to three-phase S.C. at Bus H

Balanced Load/Generation
Wind Generation Units



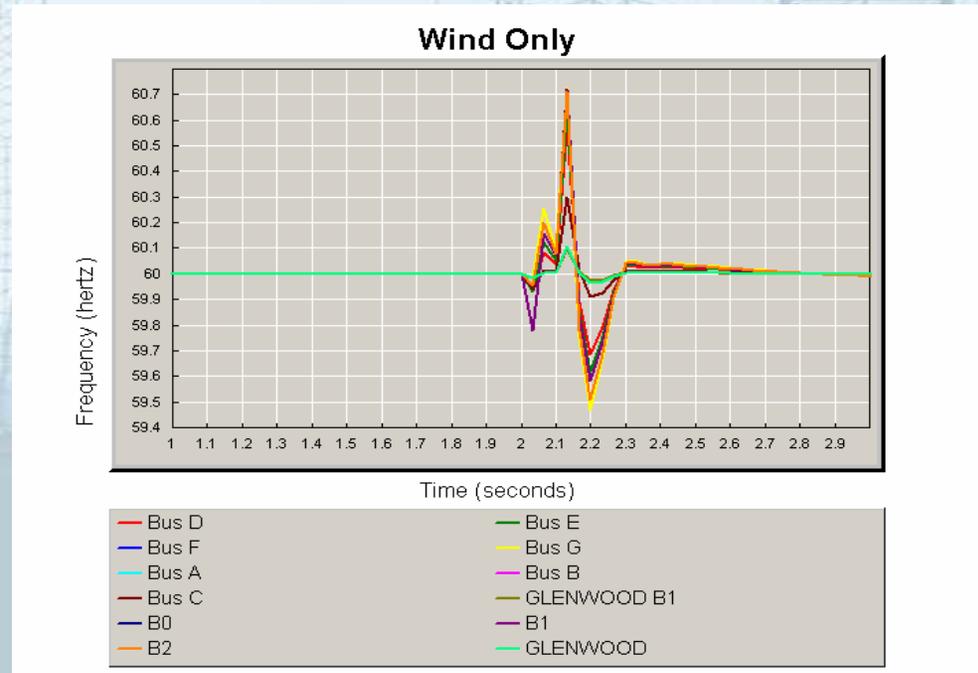
- The voltage dip vary with distance from fault
- The voltages at buses B0, F, and G drop to 0.42 pu, 0.42 pu, and 0.1 pu

B. Distribution System with Wind Units (cont.)

B.1.3 – Short-circuit condition

Frequency Response to three-phase S.C. at Bus H

Balanced Load/Generation
Wind Generation Units



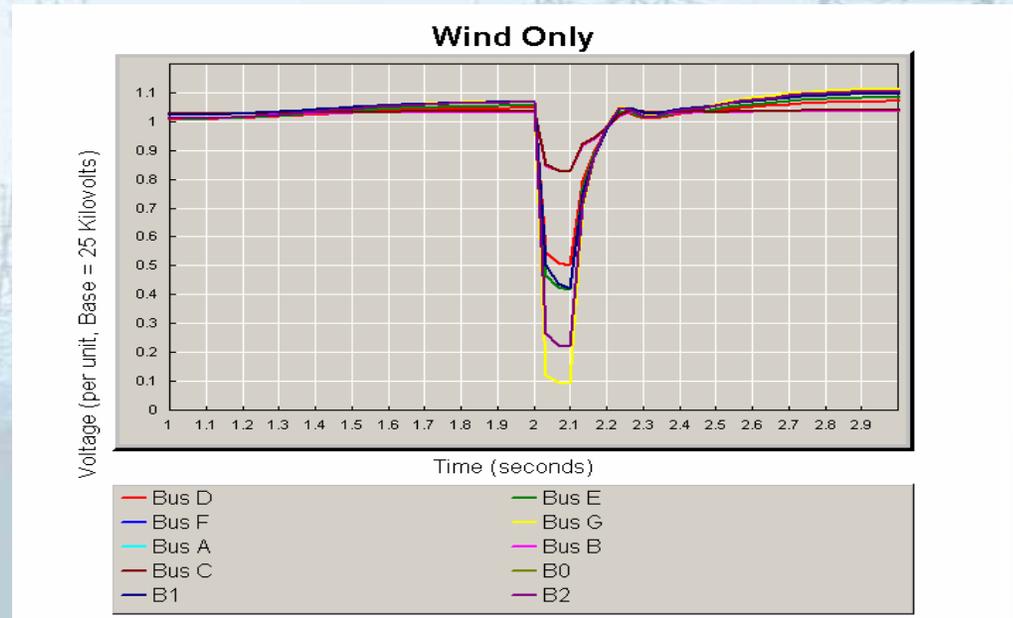
- Frequency returns to its nominal value (60Hz)
- Maximum Frequency excursion (60.7 Hz) exceeding IEEE limits

B. Distribution System with Wind Units (cont.)

B.2.1 – Short-circuit condition

Voltage Response to three-phase S.C. at Bus H

*Generation to load ratio
2/1 Wind Generation Units*



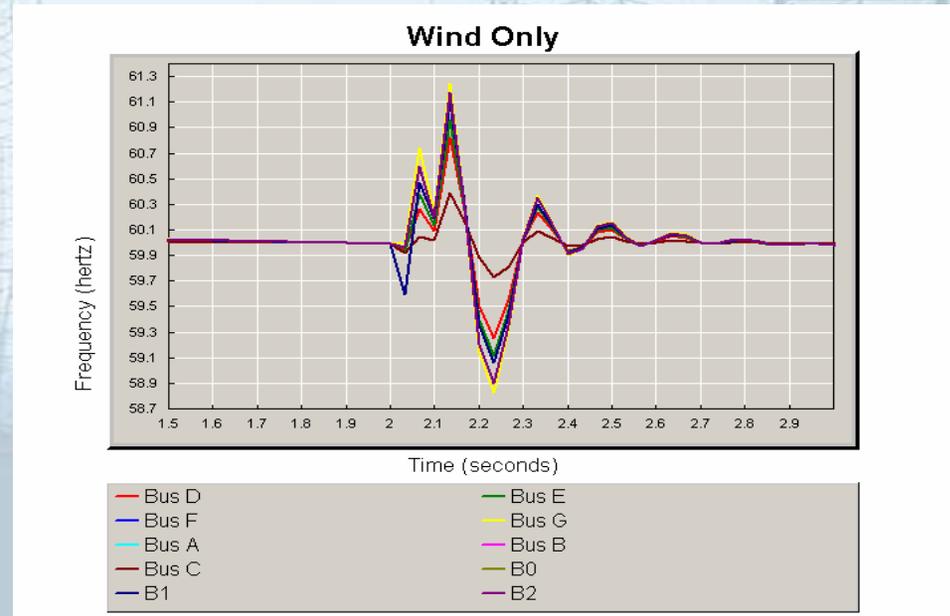
- The voltage dip varies with distance from fault
- The voltages at buses B0, F, and G drop to 0.42 pu, 0.42 pu, and 0.1 pu

B. Distribution System with Wind Units (cont.)

B.2.1 – Short-circuit condition

Frequency Response to Three-phase S.C. at Bus H

Generation to load ratio $\frac{1}{2}$



- Frequency returns to its nominal value (60Hz)
- Maximum frequency excursions (61.2 and 58.9 Hz) exceed the IEEE limits

Detection of Island Formation

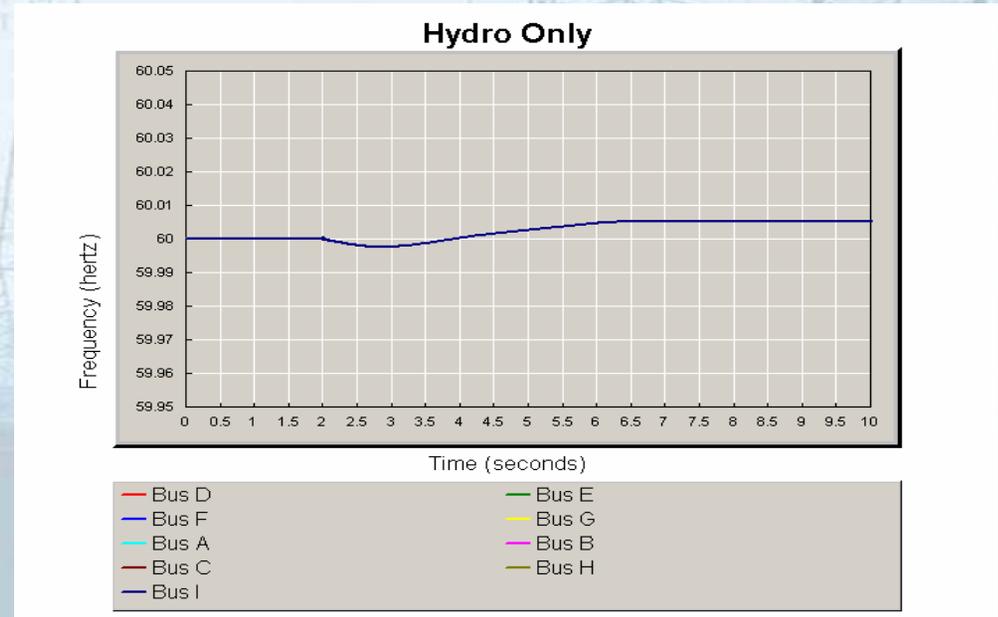
- **Distribution system response after separation**
- **DG types, operating conditions and penetration levels:**
 - A. Distribution System with Hydraulic Units:**
 - A.1 Self-Sufficient Condition
 - A.2 Under-Generating Condition
 - B. Distribution System with Diesel Units:**
 - B.1 Under-Generating Condition
 - C. Distribution System with Wind Units:**
 - C.1 Under-Compensated Condition
 - C.2 Over-Compensated Condition

A. Distribution System with Hydraulic Units

A.1 Self-sufficient condition

Frequency Response to Islanding

Self-Sufficient Condition
Hydro Units Only



- Frequency variation is insignificant
- Island formation cannot be detected based on the frequency value

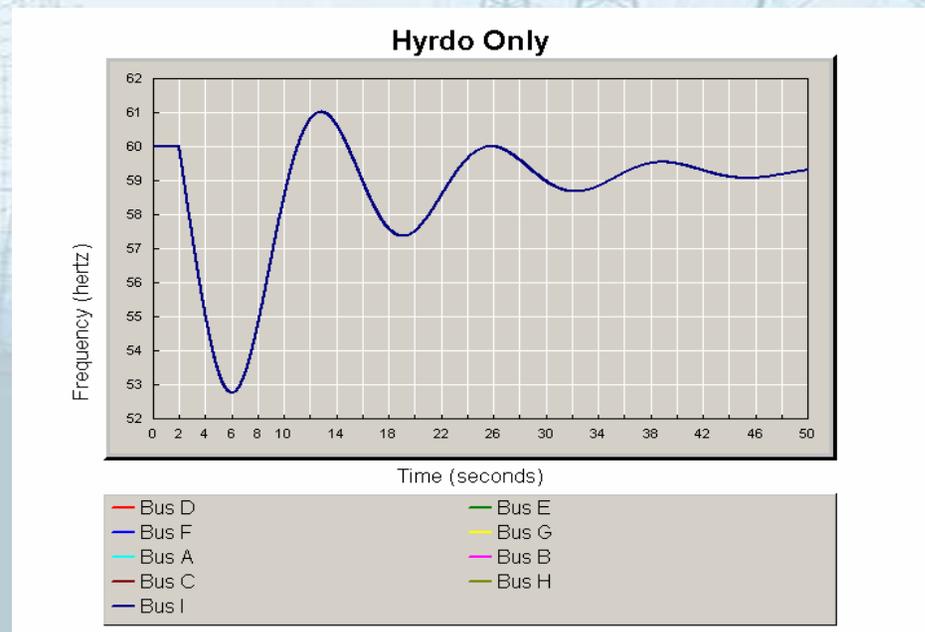
A. Distribution System with Hydraulic Units (cont.)

A.2 Under-generating condition

Two generators each producing 1.56 MW

Frequency Response to Islanding

Generation/Load Ratio 2/3



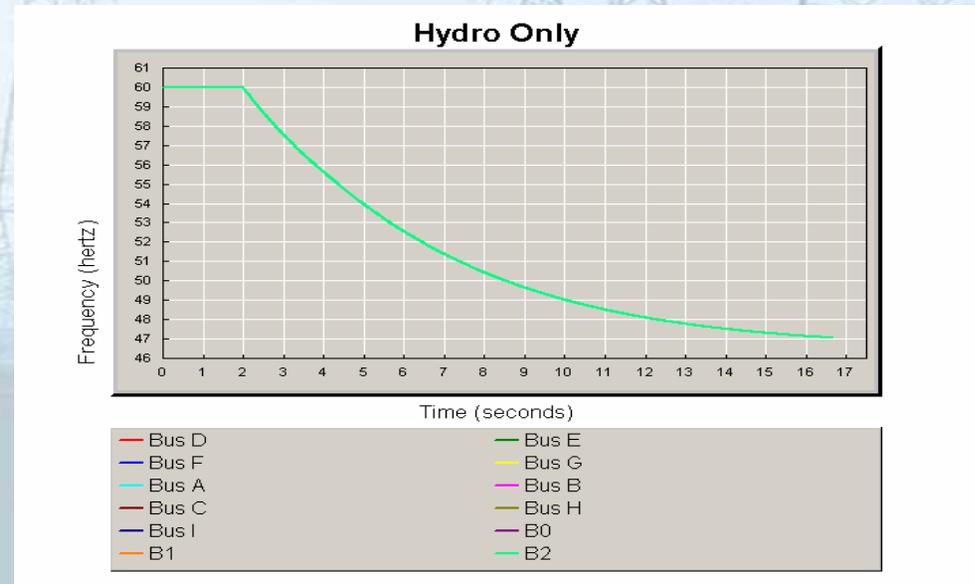
- Large variation in the frequency of 55.6 Hz, Island can be detected

A. Distribution System with Hydraulic Units (cont.)

A.2 Under-generating condition with disabled governor

Frequency Response to Islanding - No Governor

Generation/Load Ratio 2/3



- Frequency decreases monotonically
- The frequency deviation exceeds the IEEE limits

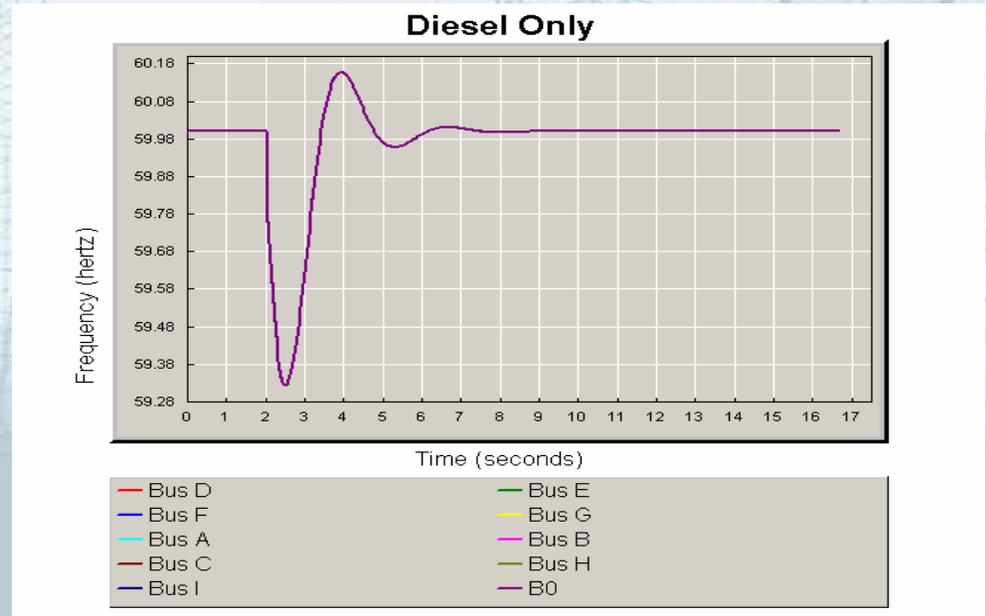
B. Distribution System with Diesel Units

B.1 Under-generating condition

Frequency Response to Islanding

Generation/Load Ratio $\frac{1}{2}$

Diesel Units Only

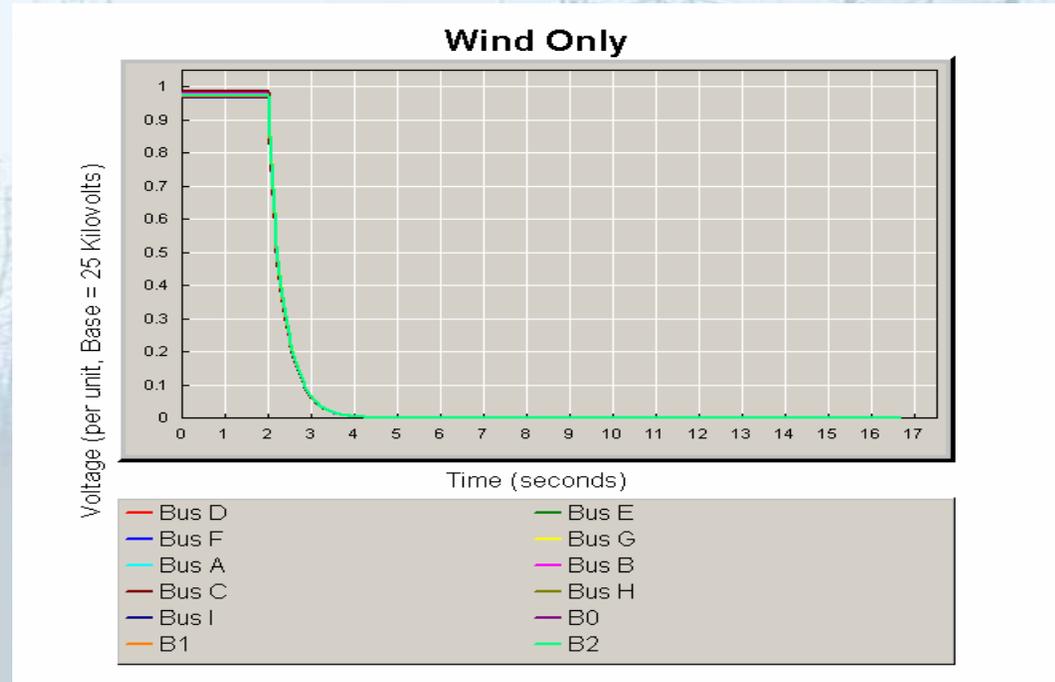


- Small variation in the frequency (59.32 Hz)
Island cannot be detected.
- Frequency returns to nominal value of 60 Hz

C. Distribution System with Wind Generating Units

C.1 Under-compensated condition

**Voltage Response
to Islanding**
Balanced Condition
Wind Units Only

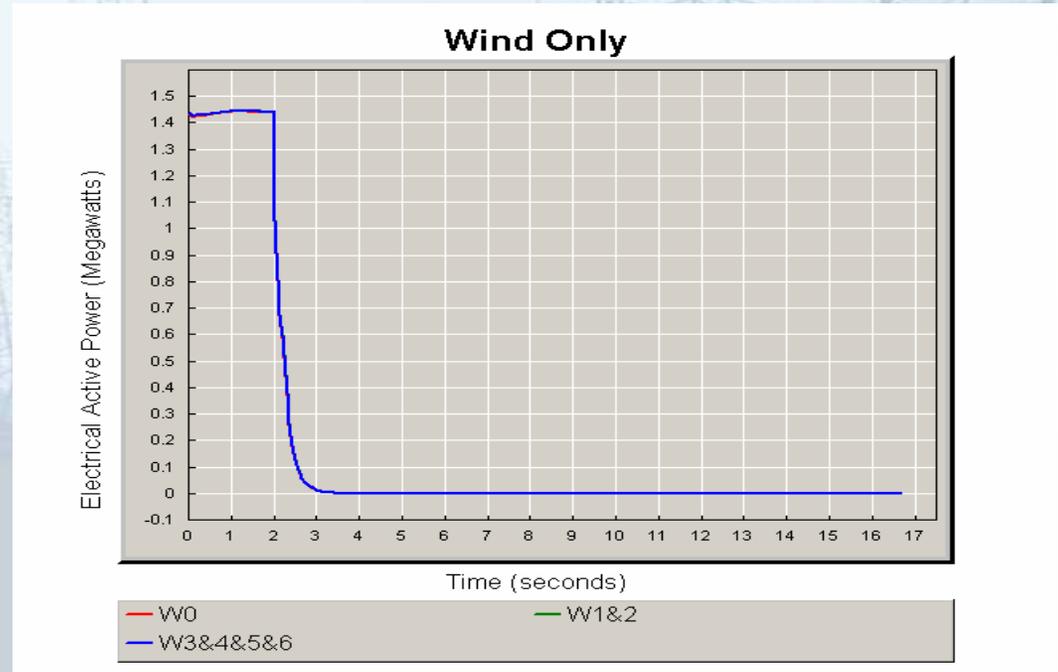


- Voltages decrease monotonically to zero
- The voltage exceeds IEEE limits for island formation

C. Distribution System with Wind Units (cont.)

C.1 Under-compensated condition

**Real-Power Unit
Response to
Islanding**
Balanced Condition

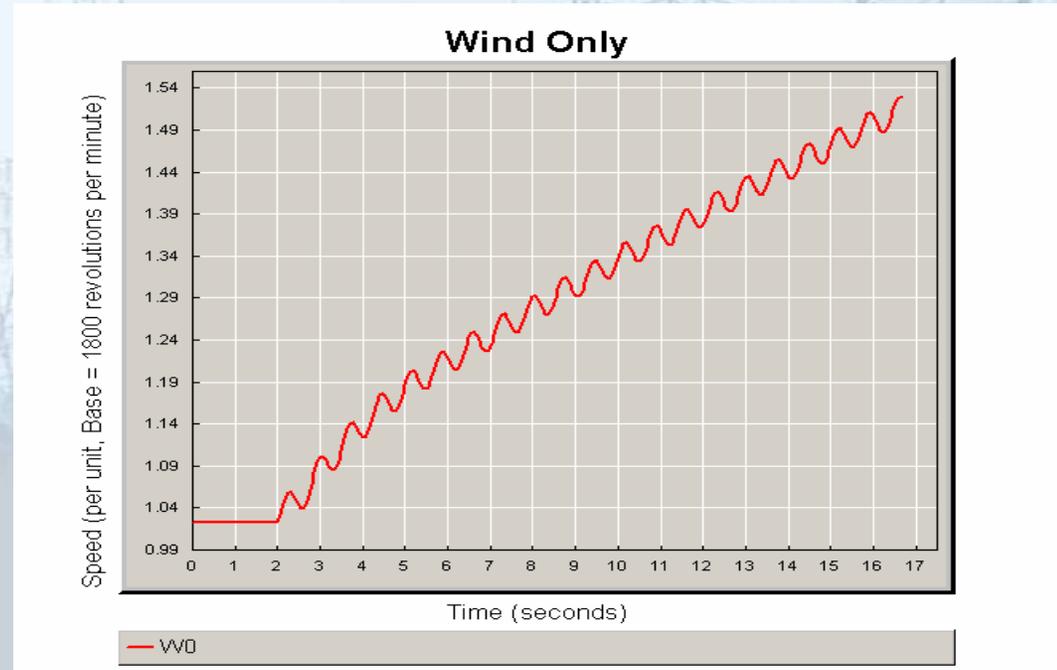


- System voltage drops to zero and generator outputs also drop to zero

C. Distribution System with Wind Units (cont.)

C.1 Under-compensated condition

Frequency Response to Islanding *Balanced Condition*

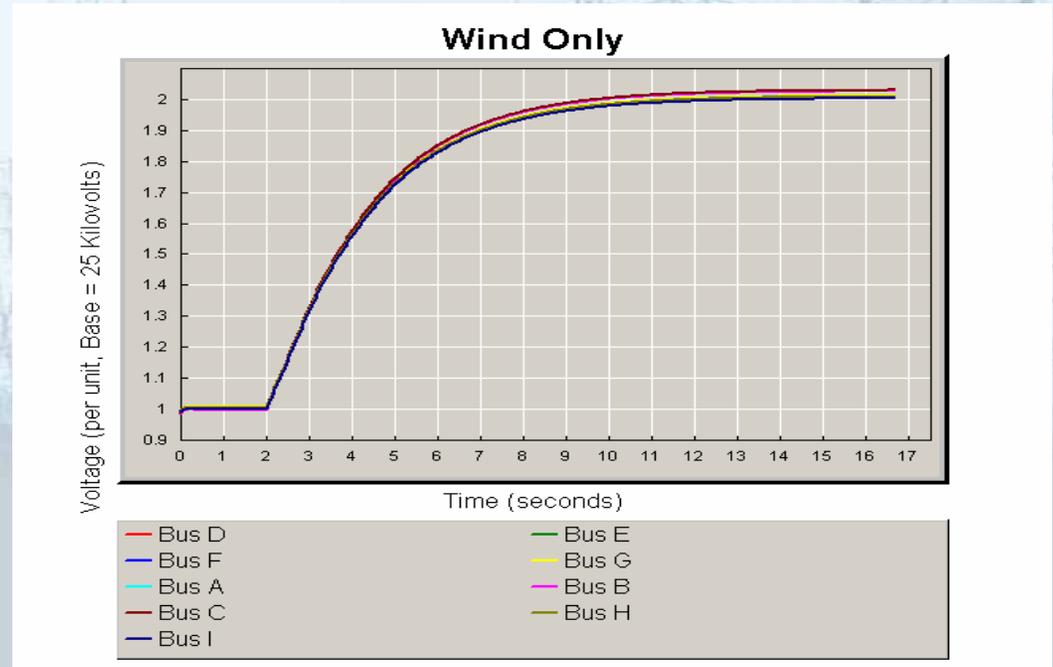


- Constant wind, mechanical power remains constant
- System frequency (speed) increases monotonically

C. Distribution System with Wind Units (cont.)

C.2 Over-compensated condition

Voltage Response to Islanding
Over-Compensated Condition – 0.43 MVAR



- Bus voltages increase monotonically
- Voltages exceed the limits for island detection

■ Feasibility of Island Mode Operation:

A. Distribution System with Hydraulic Units:

A.1 Over-Generating Condition with Under-Damped Governor

A.2 Over-Generating Condition with Generation/Load 10 MW/4.6 MW

A.3 Under-Generating Condition with Generation/Load 1.5 MW/4.6 MW

B. Distribution System with Diesel Units:

B.1 Over-Generating Condition with
Generation/Load 10 MW/ 4.6 MW

B.2 Under-Generating Condition with
Generation/Load 1.5 MW/4.6 MW

C. Distribution System with Hydro and Wind Units

D. Distribution System with Diesel and Wind Units

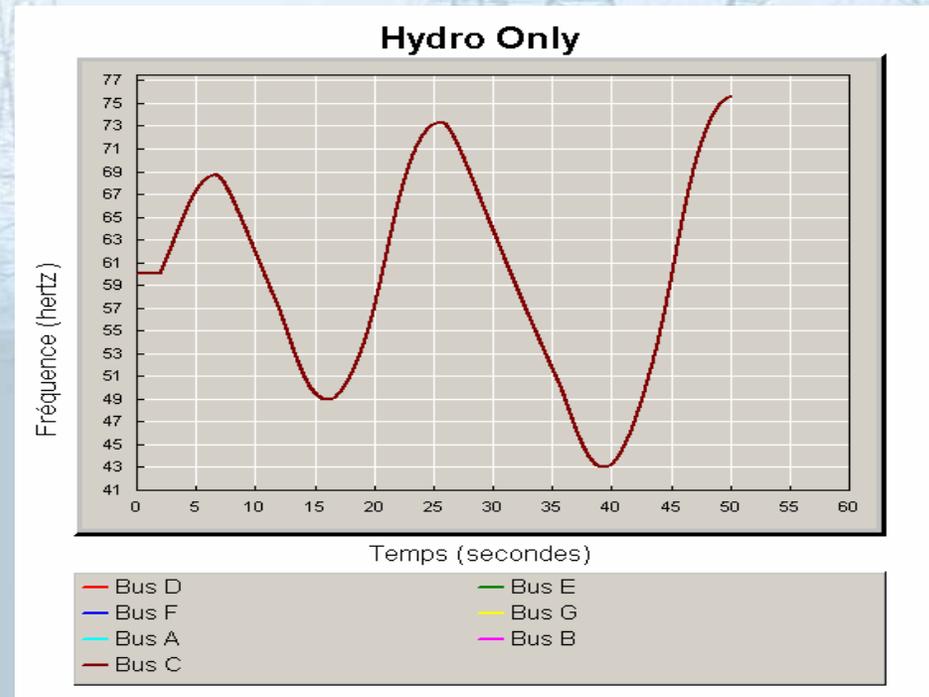
A. Distribution System with Hydraulic Units

A.1 Over-generating condition with under-damped governor

Frequency Response to Islanding

Generation/Load Ratio 2/1

- Unstable island



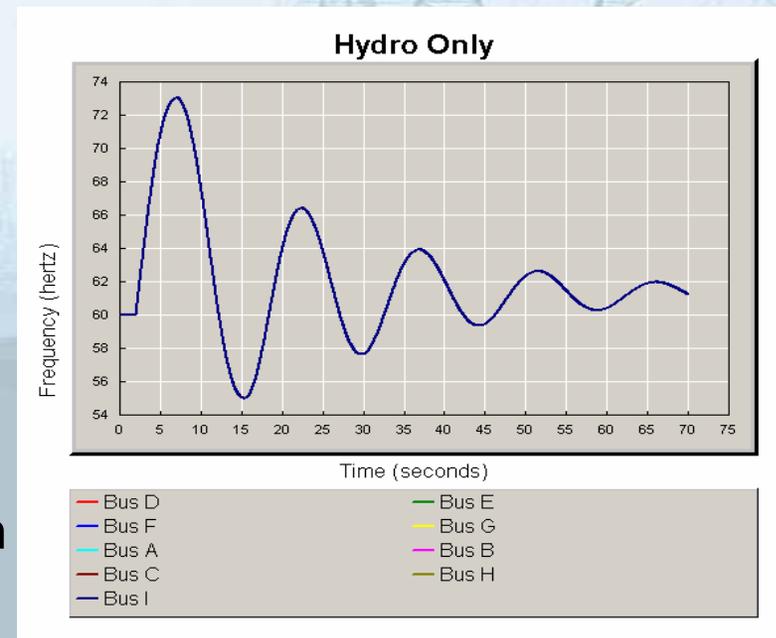
A. Distribution System with Hydraulic Units (cont.)

A.2 Over-generating condition with generation/load 10 MW/4.6 MW

Frequency Response to Islanding

Generation/Load 10 MW/4.6 MW

- The frequency excursion reaches 73 Hz
- The generators trip on over-speed protection of the turbine set at 72 Hz



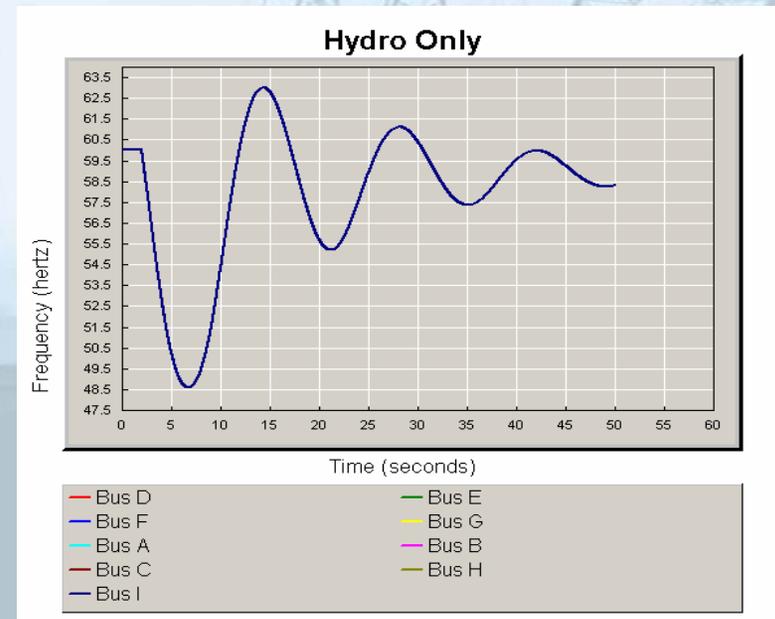
A. Distribution System with Hydraulic Units (cont.)

A.3 Under-generating condition with generation/load 1.5 MW/4.6 MW

Frequency Response to Islanding

Generation/Load 1.5 MW/4.6 MW

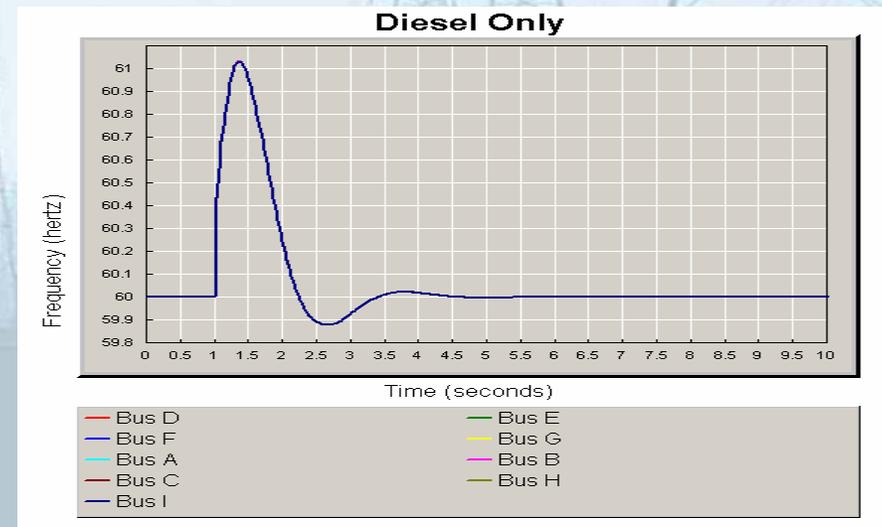
- The frequency excursion reaches 48.5 Hz
- Frequency is very close to the under-speed protection set at 48 Hz



B. Distribution System with Diesel Units

B.1 Over-generating condition with generation/load 10 MW/4.6 MW

**Frequency Response
to Islanding**
*Generation/Load
10 MW/4.6 MW*

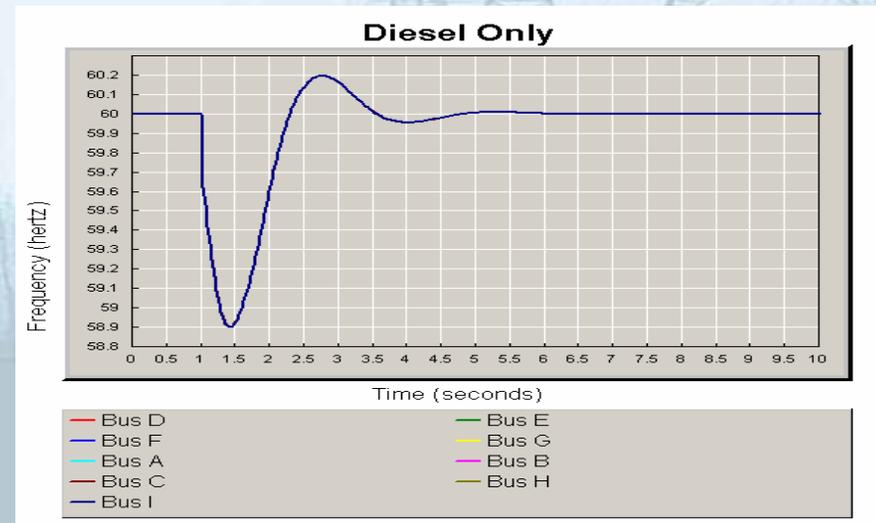


- Maximum frequency 61.04 Hz
- Not large enough to trigger over-speed protection
- System frequency returns to 60 Hz

B. Distribution System with Diesel Units (cont.)

B.2 Under-Generating Condition with Generation/Load 1.5 MW/4.6 MW

Frequency Response to Islanding
Generation/Load 1.5 MW/4.6 MW



- Maximum frequency 58.9 Hz
- Not large enough to trigger over-speed protection
- System frequency returns to 60 Hz

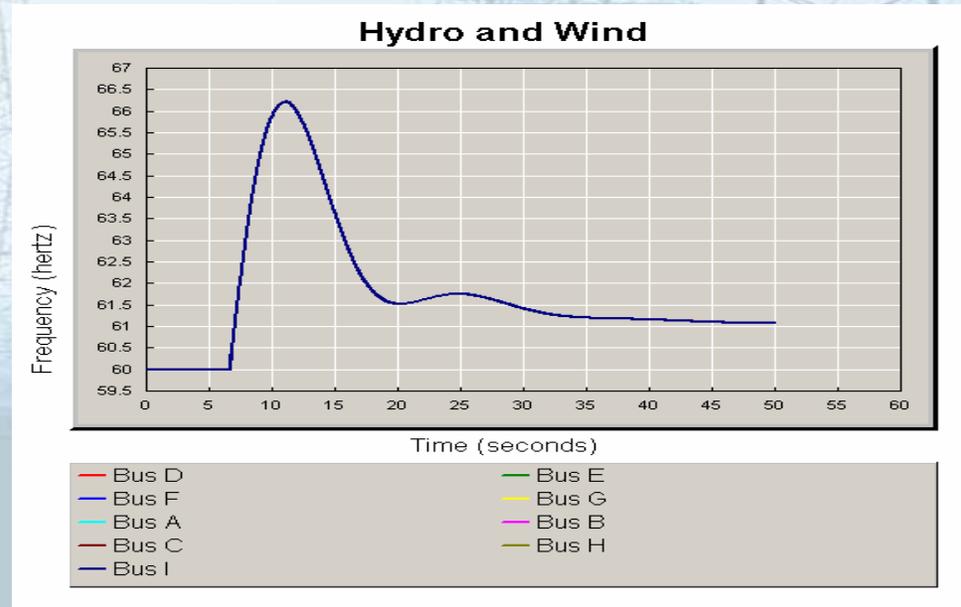
C. Distribution System with Hydro and Wind Units

C. Over-Generating Condition with Generation/Load 5.9 MW/4.6 MW

Frequency Response to Islanding

Hydro Units 3 MW, Wind Units 2.9 MW

- Maximum 66.3 Hz
- Not high enough to trigger protection
- Steady-state frequency 61 Hz

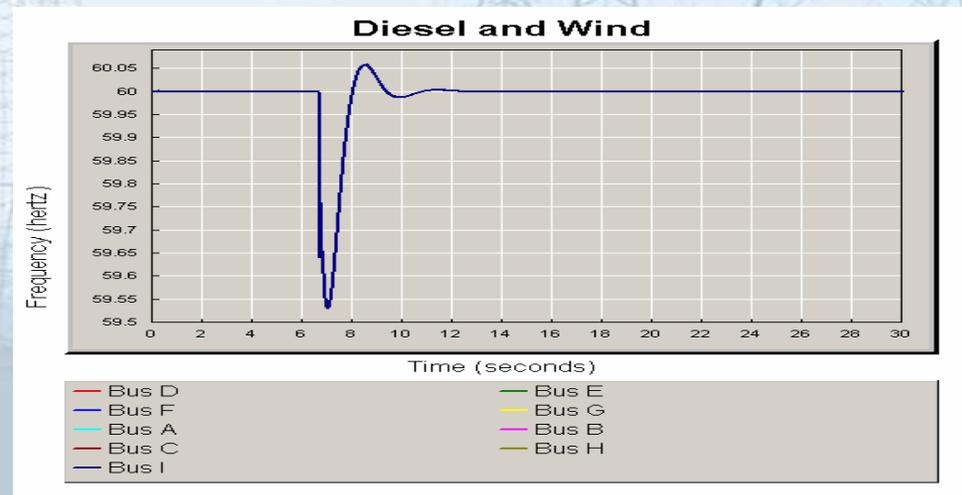


D. Distribution System with Diesel and Wind Units

D. Under-Generating Condition with Generation/Load 3.9 MW/4.6 MW

Frequency Response To Islanding

Diesel Units 1 MW, Wind Units 2.9 MW



- Maximum frequency variation 59.53 Hz
- Not low enough to trigger protection
- The system frequency returns to 60 Hz

Conclusions

- **Implementing distributed generation changes the way distribution systems are planned and operated**
- **Enhanced analytical tools capable of meeting the emerging requirements need to evolve**
- **CYME – NRCan collaboration**
 - Tool enhancement
 - Case studies
- **Ongoing activities**
 - Expanded DG model library
 - More case studies for illustration/education